

MULTI-HULL SHIPS: strength, structure mass

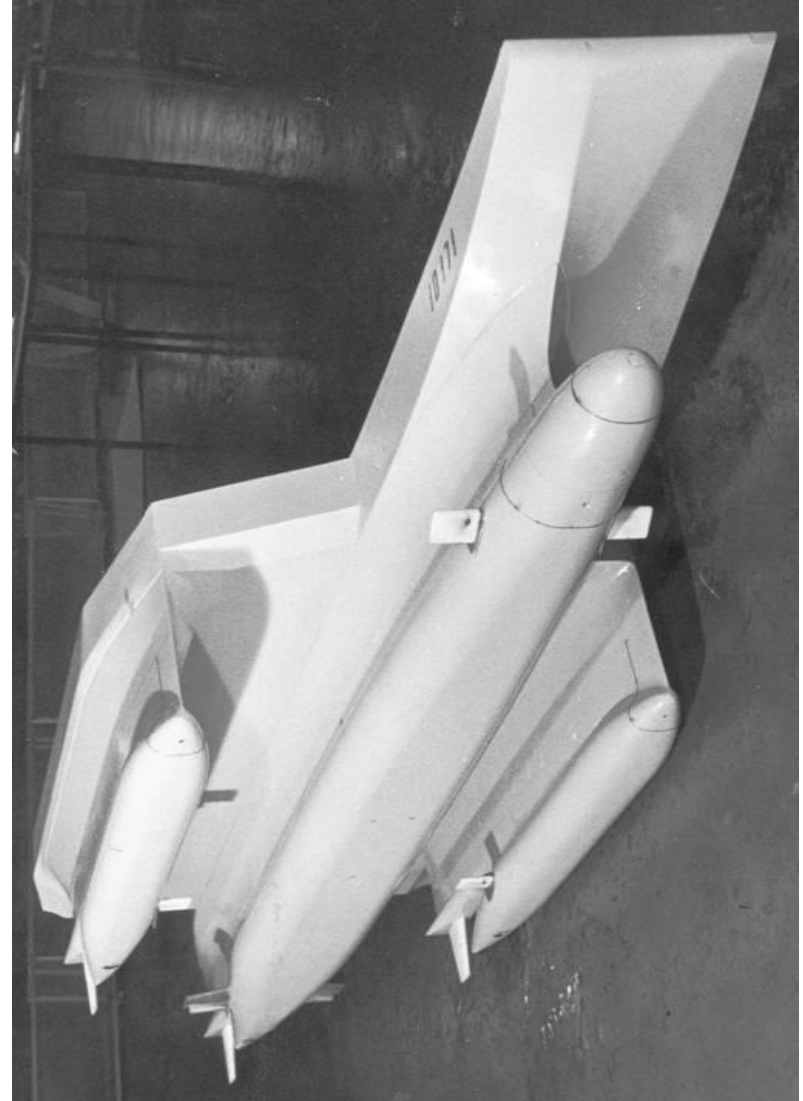
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Dr. Scs., Dr. Phil.

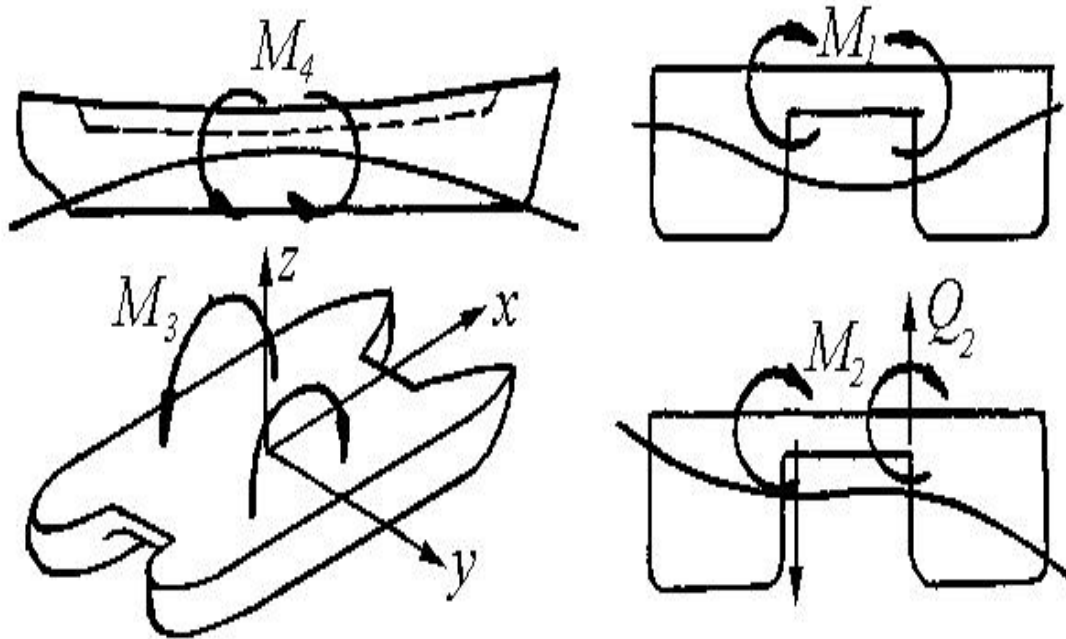
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“Specificity and designing
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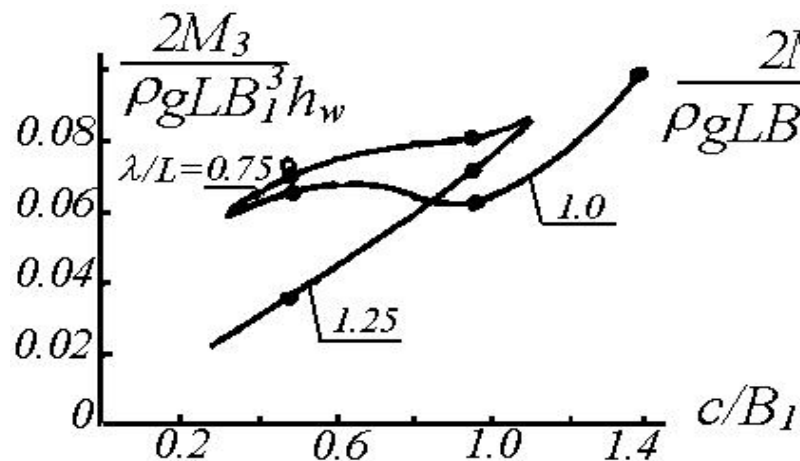
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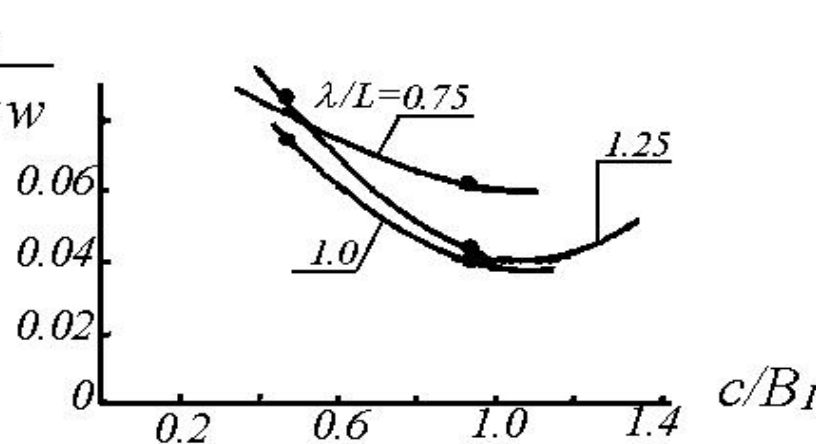
Simplified scheme for catamaran external loads [1].



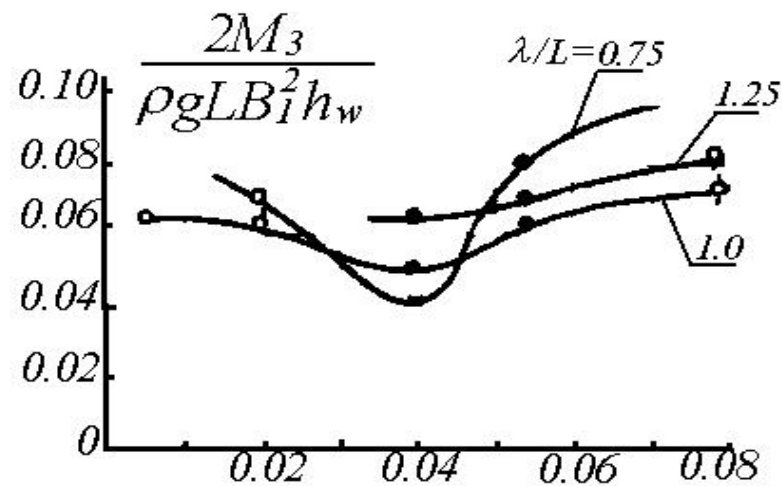
Some experimental data on clearance influence on external bending moments [1].



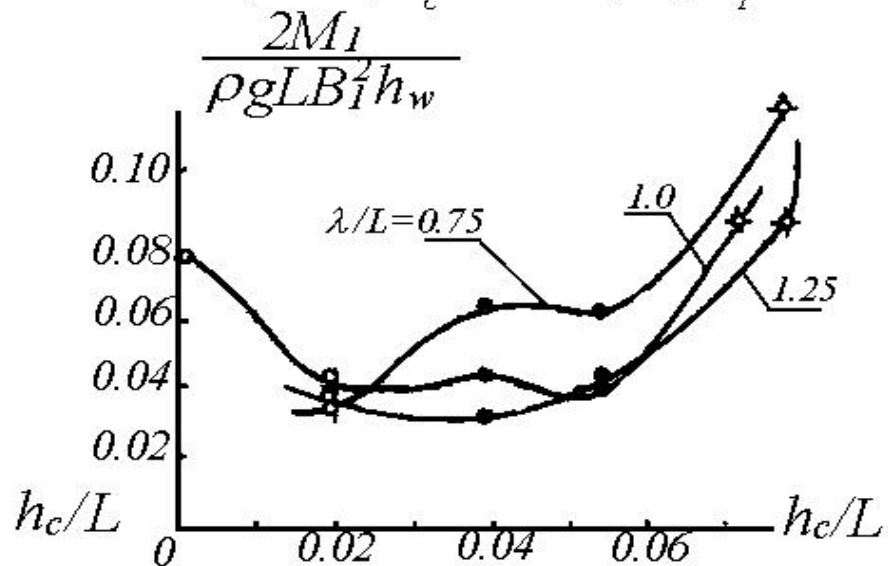
$\varphi = 60^\circ; h_c/L = 0.055; z_0/B_1 = 0.54$



$\varphi = 90^\circ; h_c/L = 0.055; z_0/B_1 = 0.54$



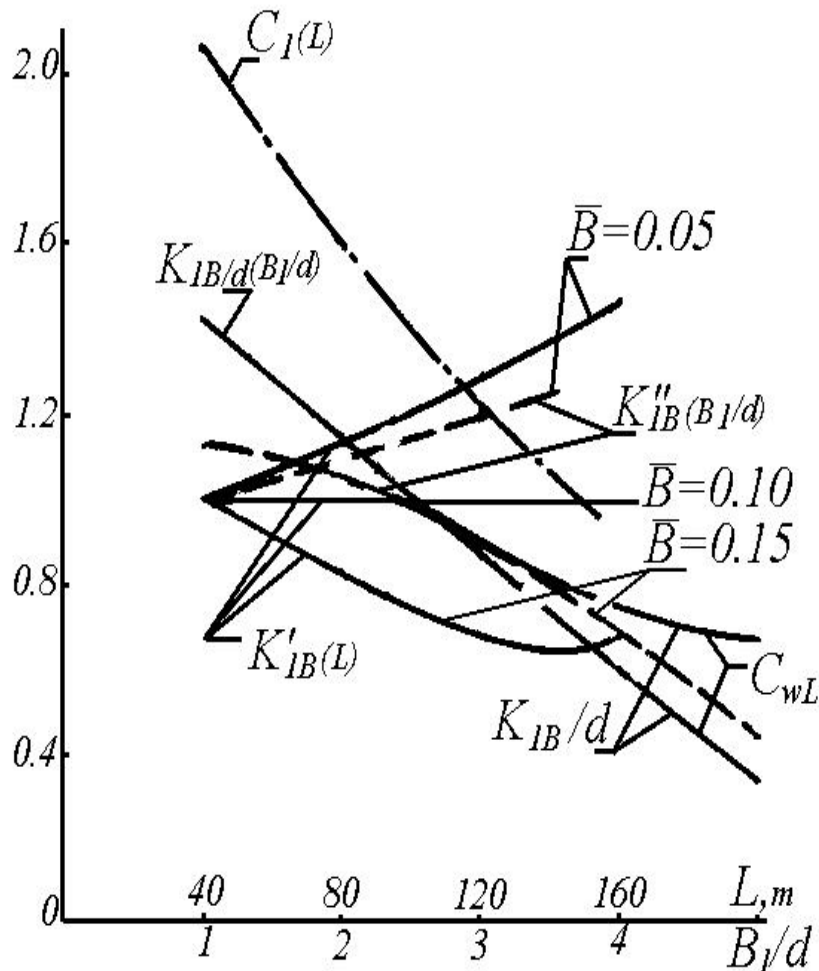
$\varphi = 60^\circ; c/B_1 = 0.95$



$\varphi = 90^\circ; c/B_1 = 0.95$

$$M_1 = K_{1B/d} K'_{1B} K''_{1B} C_1 C_{WL}^{0.4} \rho g B_1 d L z_0$$

An example of the data for approximate estimation of catamaran external loads [1]: symmetrical moment M_1 .



$$M_1 = K_{1(B/d)} * K'_{1B} * K''_{1B} * C_1 * C_{WL}^{0.4} * \rho g B_1 d L z_0$$

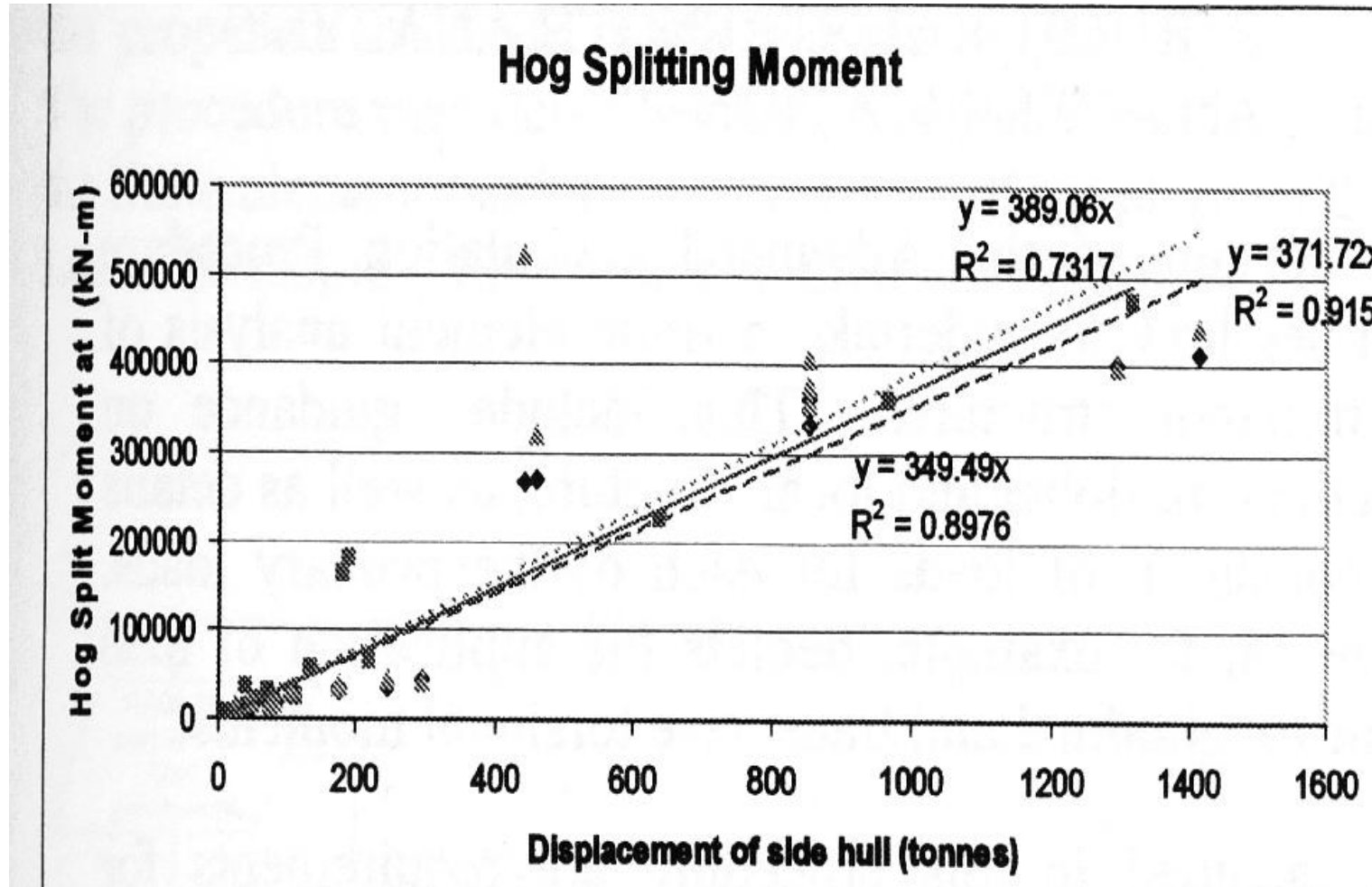
Here L , B , d – a hull dimensions;

C_{WL} – a hull water-plane area coefficient;

ρ – water density;

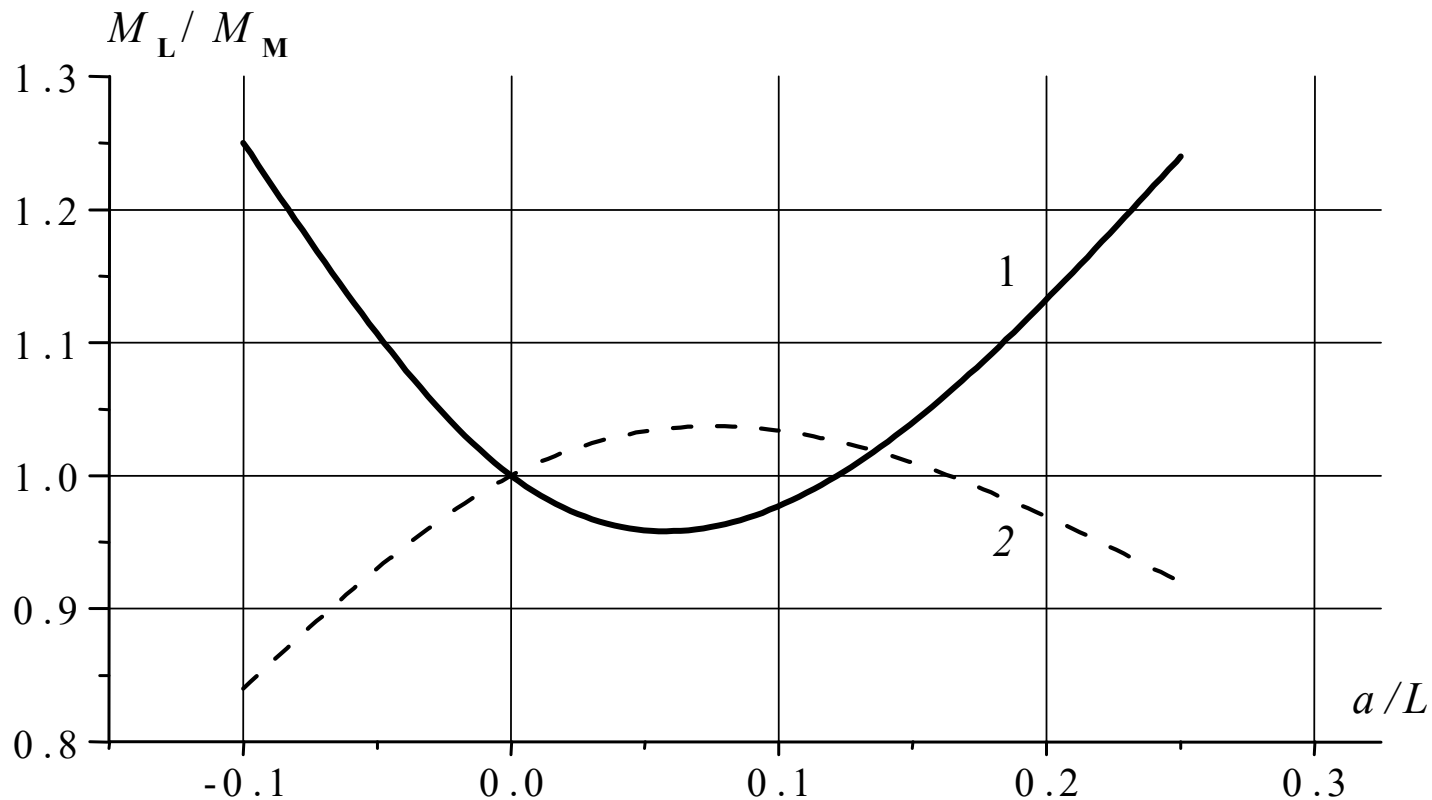
g – acceleration of free drop;

An example: transverse moment on outrigger ship, outriggers on middle [2]

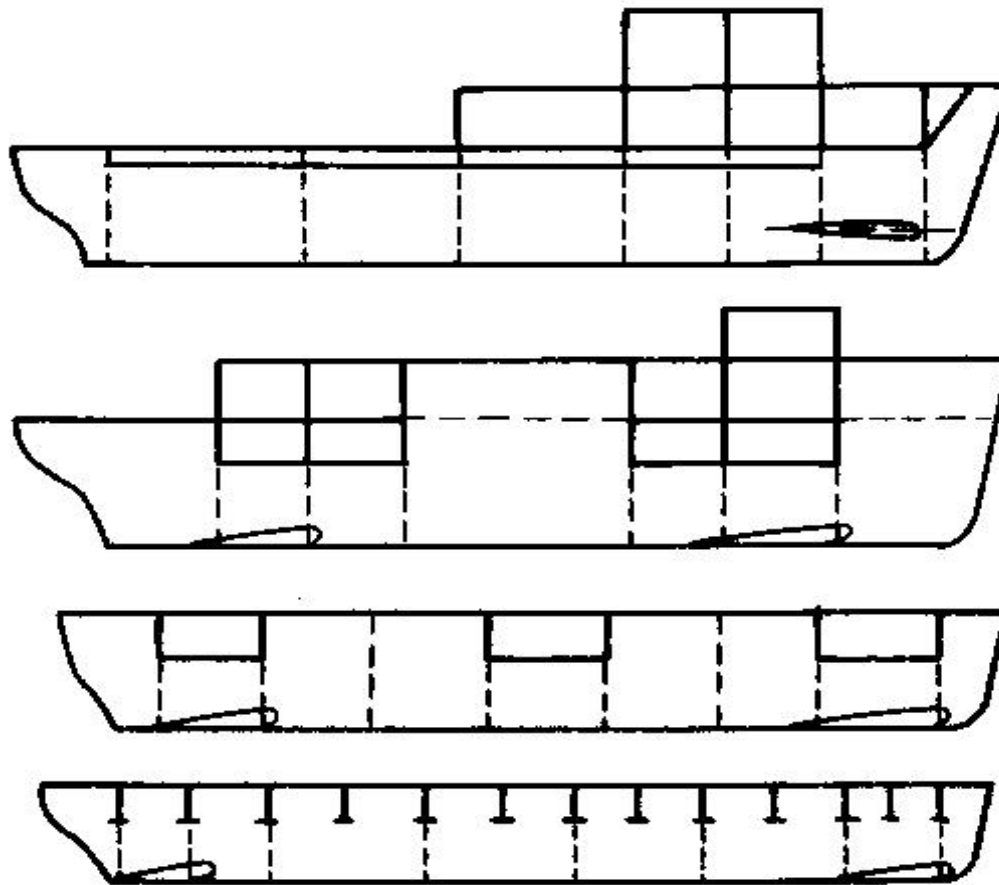


Effect of outriggers' position on longitudinal hogging (1) and sagging (2) bending moment, M_L , relative to that when outriggers at amidships, M_M , after [2];

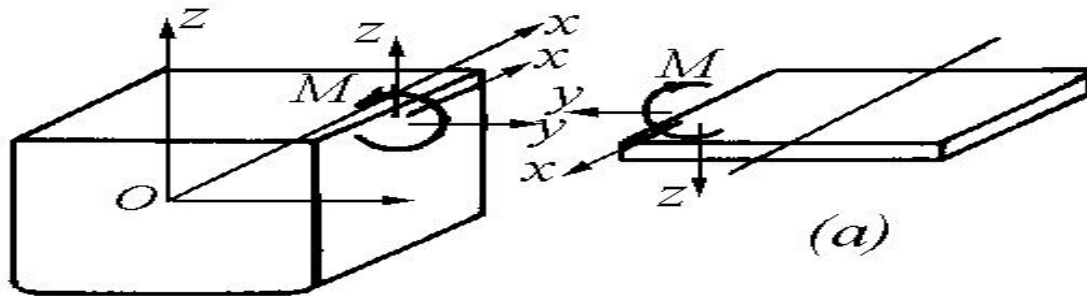
**here a = distance between midship stations of outriggers and main hull,
negative for outriggers shifted aft.**



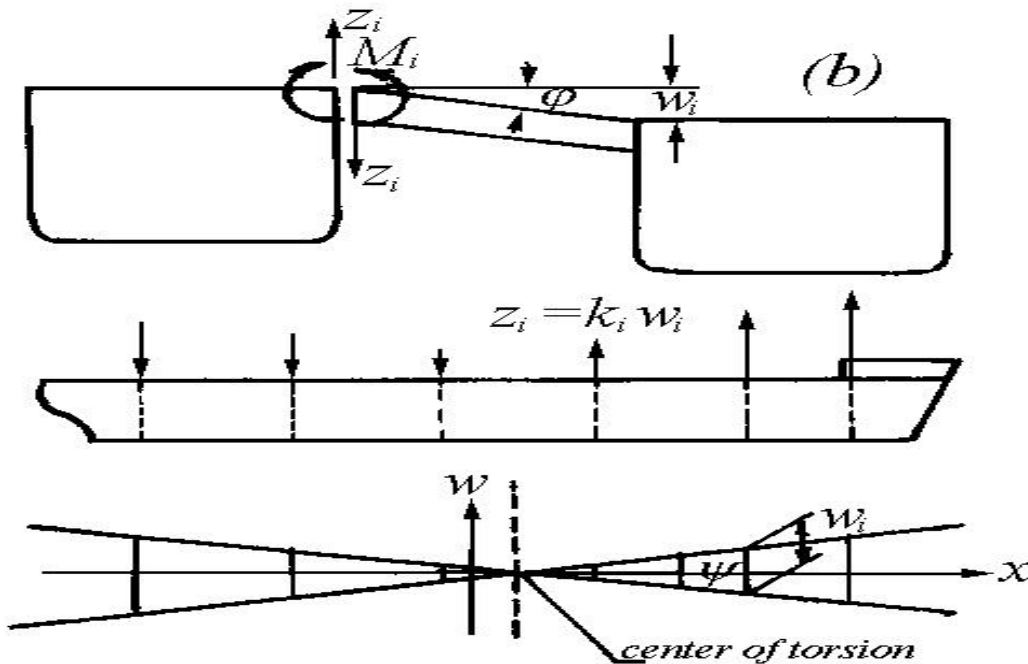
Some examples of applied types of a catamaran cross structure [1].



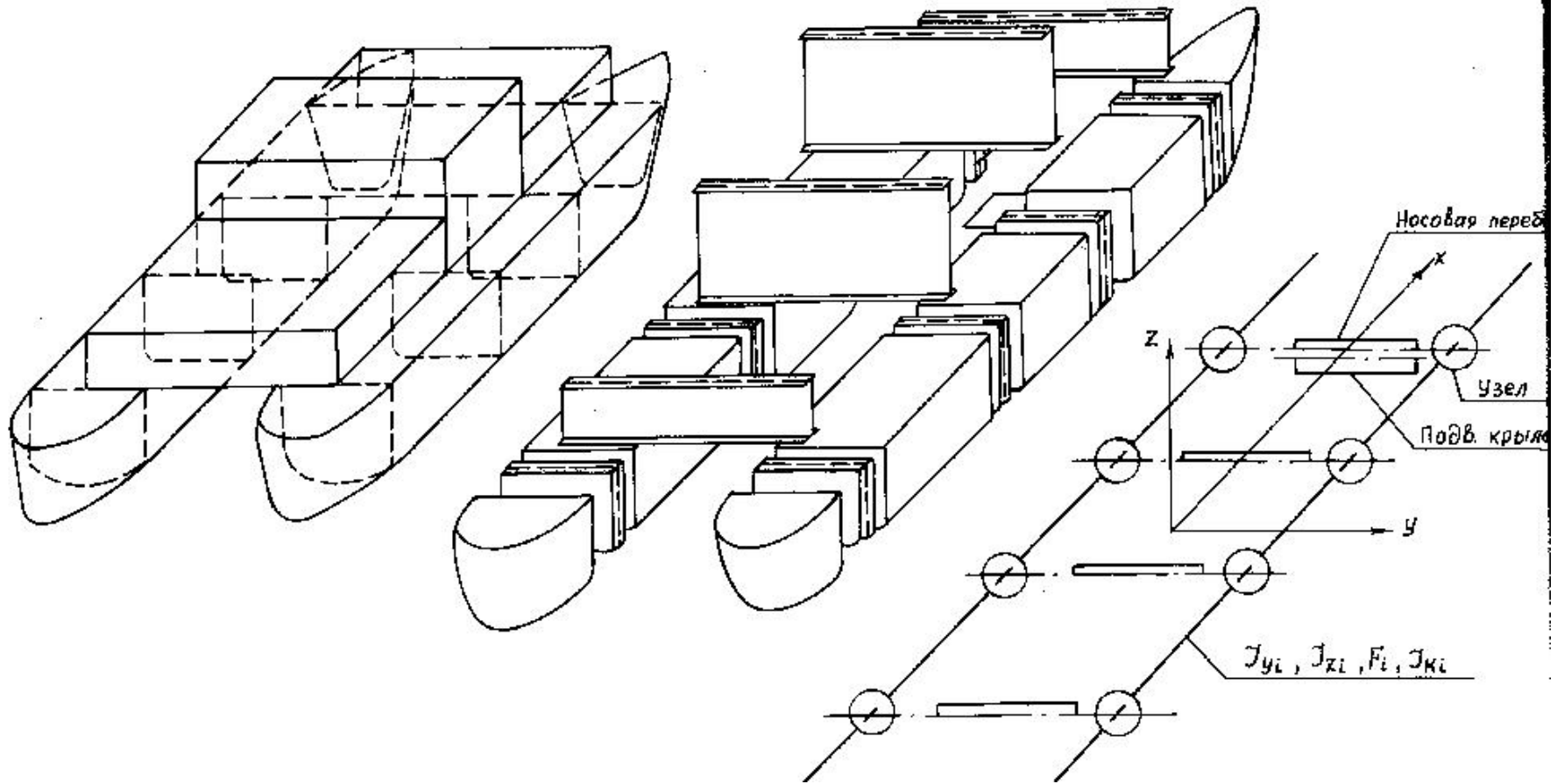
Schematics of structural response analysis in different solutions [1]:



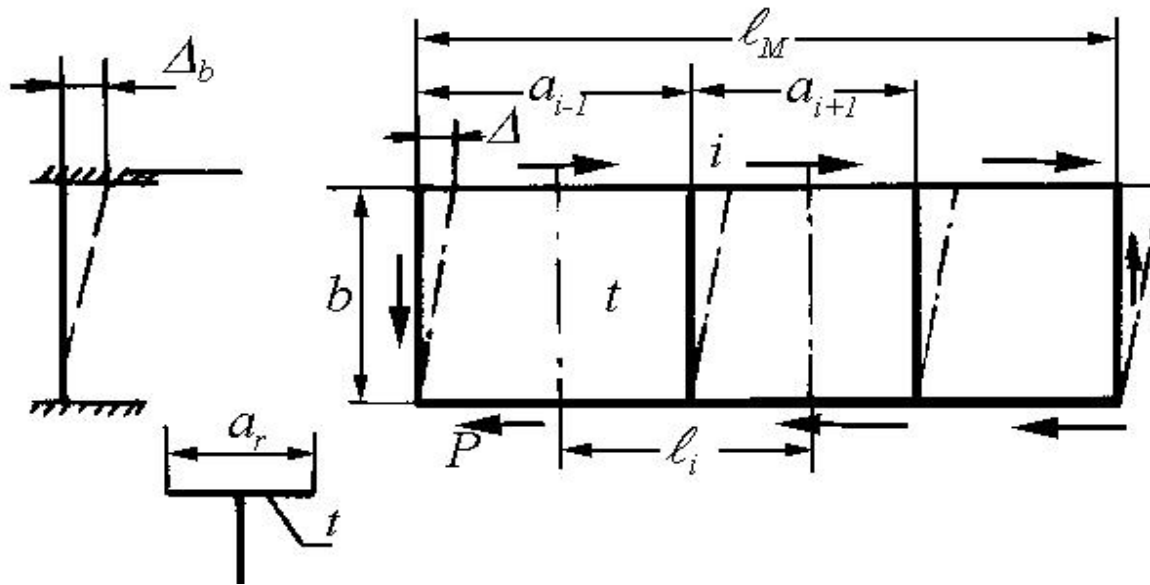
- a) - after Galakhov & Volkova [1] for the structure in Slide 5, bottom;
- b) after Ferin & Belenky [1] for the structure in Slide 5, top.



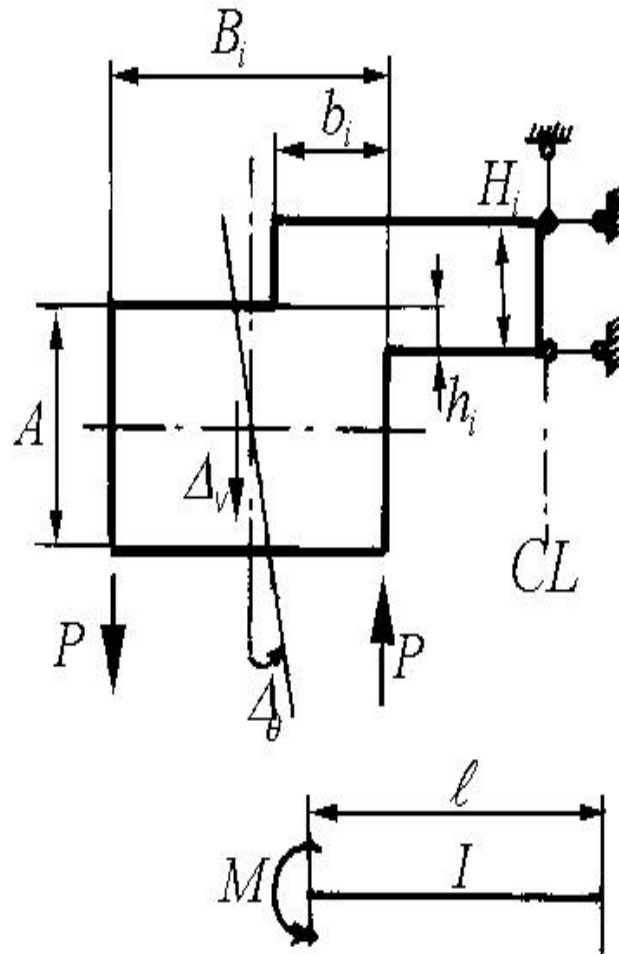
Stages of a catamaran structure idealization [1]



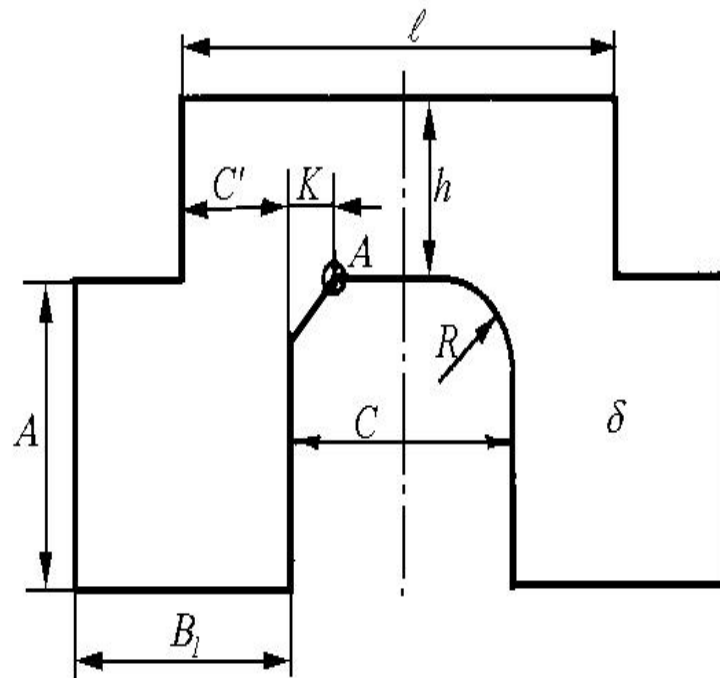
Idealization of deck plating by a beam simulating its shear loading [1]



Catamaran girder idealization [1].



Tested model of girder [1].

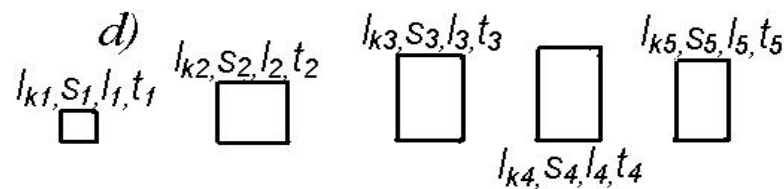
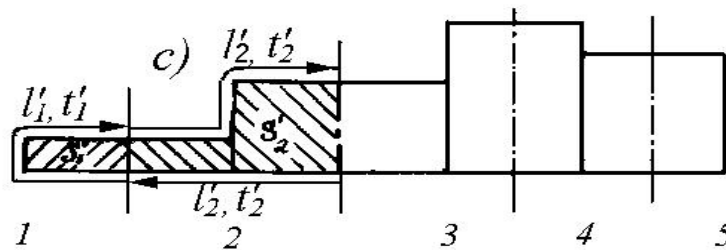
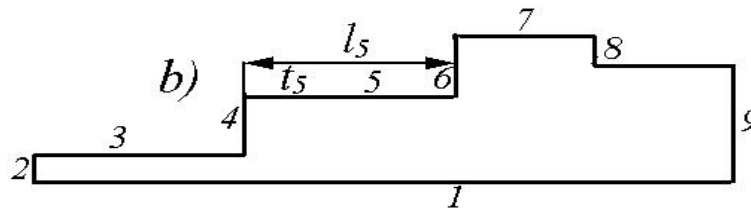
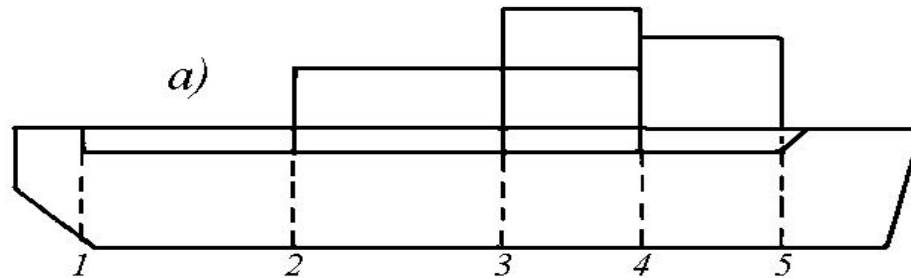


Idealization of torsional rigidity of the bridge [1]:

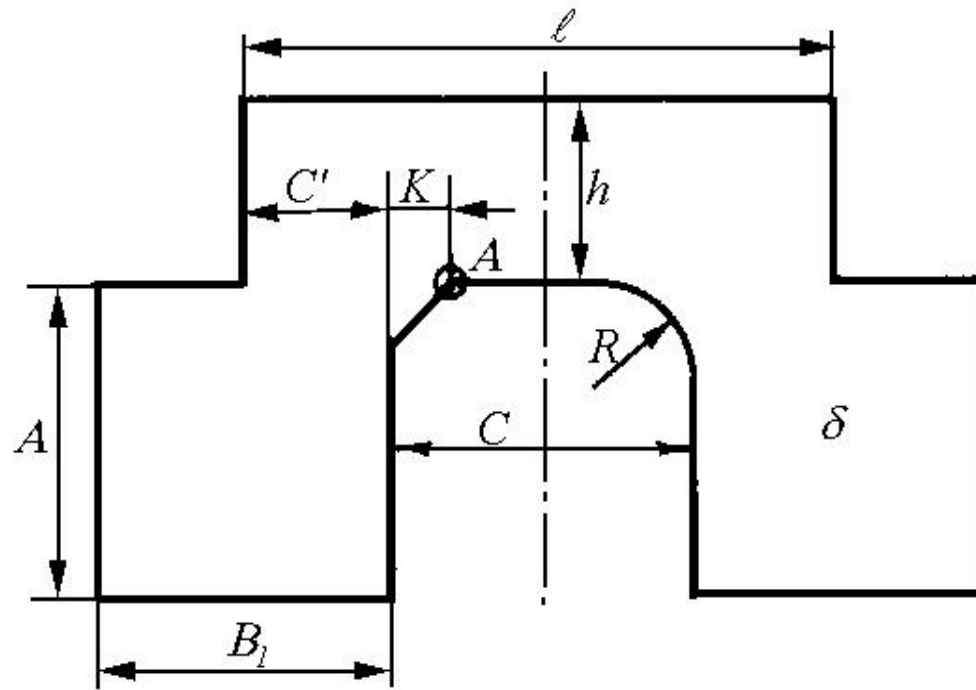
a – actual cross section,

b - contour of the bridge as a whole,

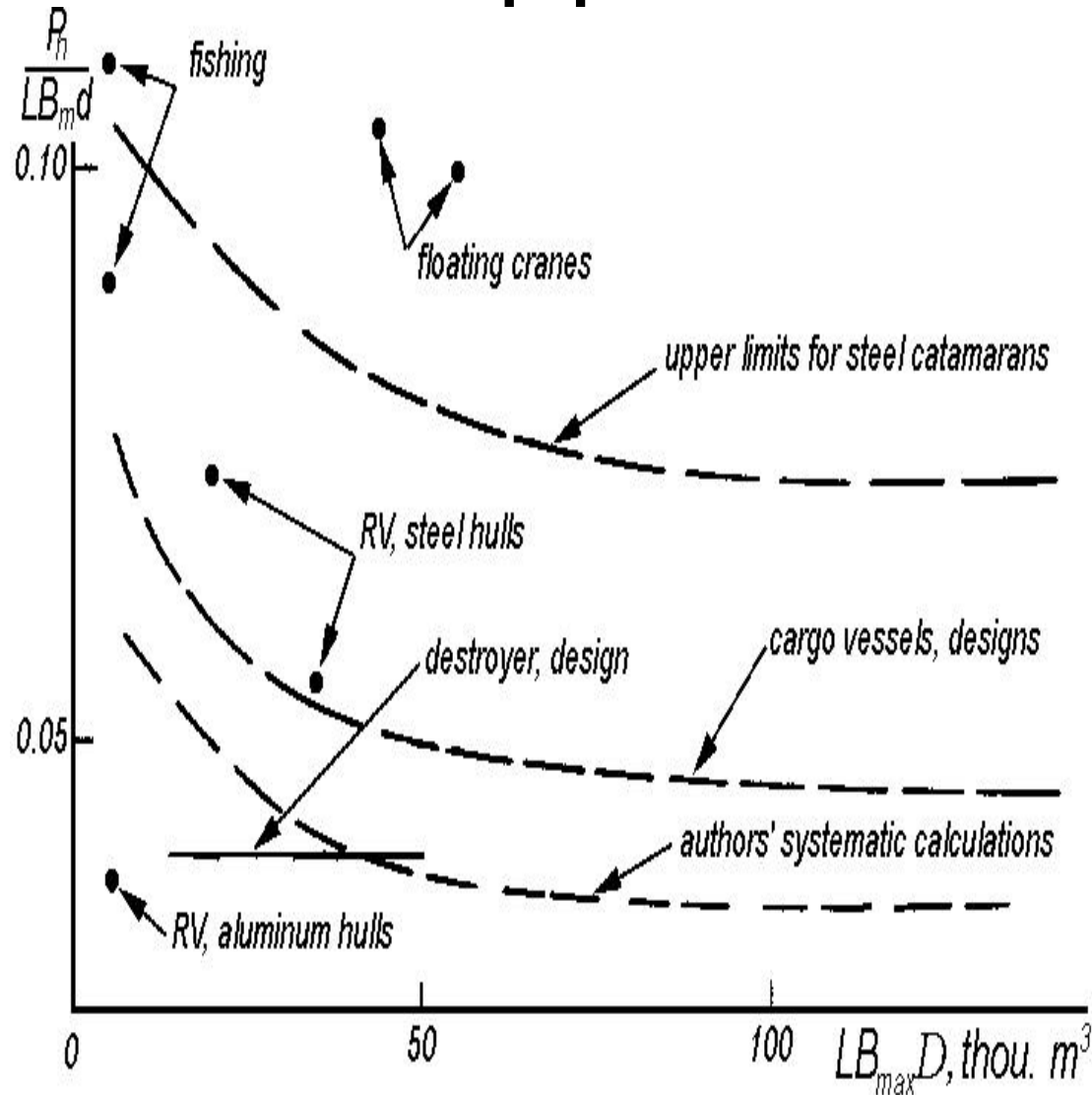
c, d - characteristics of torsional rigidity of individual girders



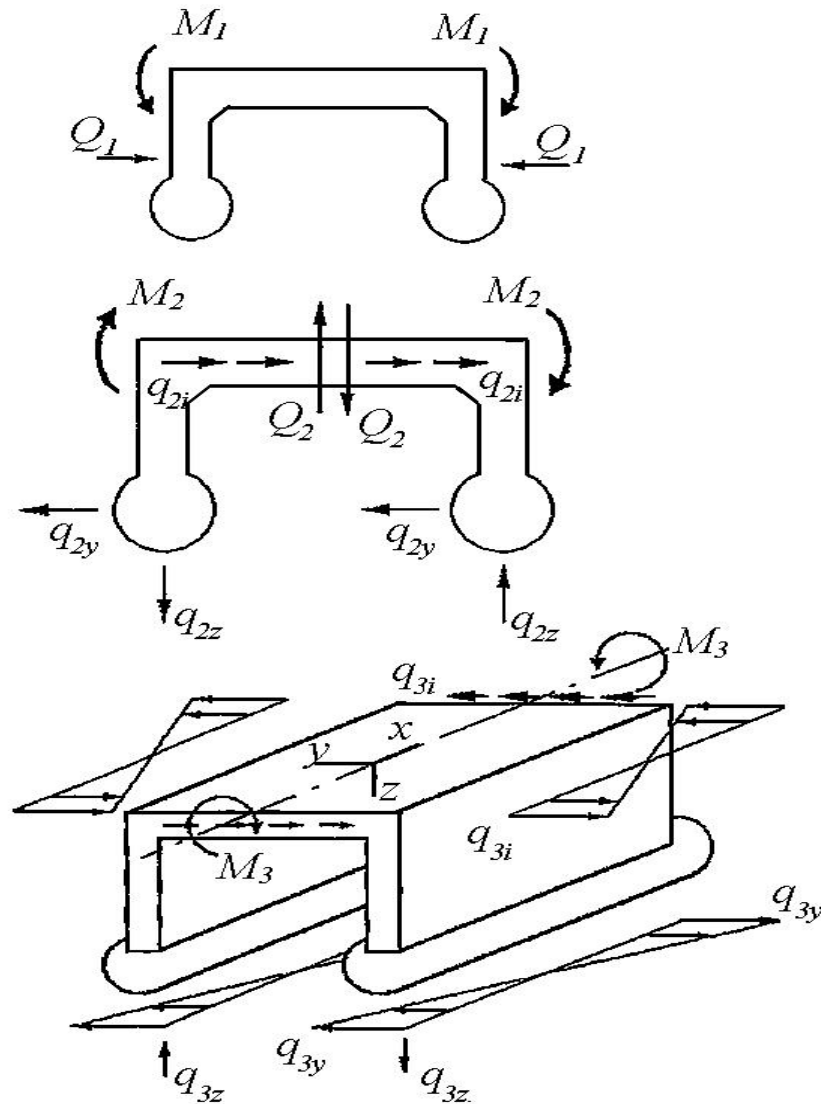
Bridge model for stress distribution study [1]



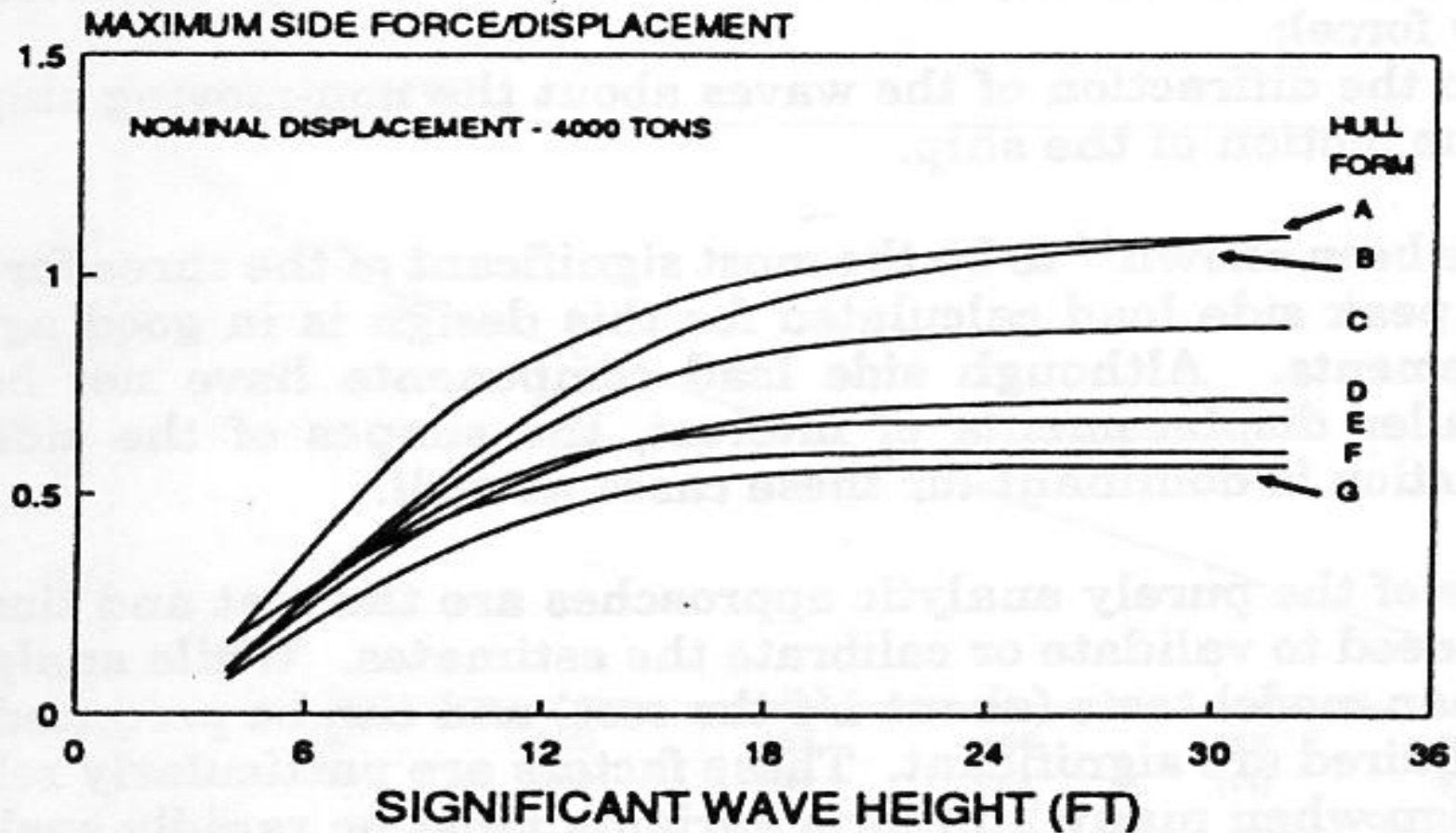
Generalized data on catamaran hull weight, [1].



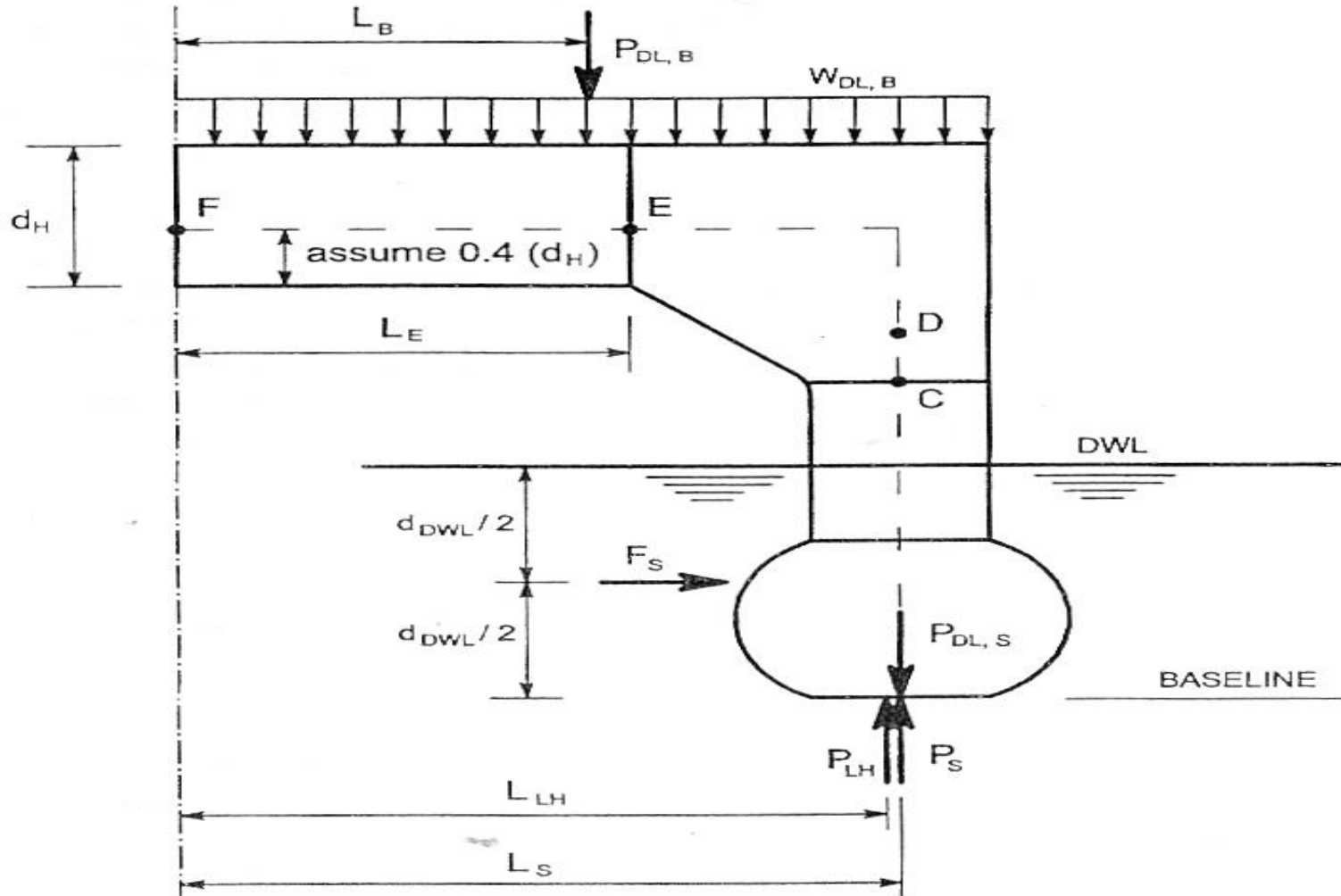
SWATH external loads [3].



Experimental data on side force at rest [3].



The scheme of side force F_S generation – the main external load for early stage of designing [2]

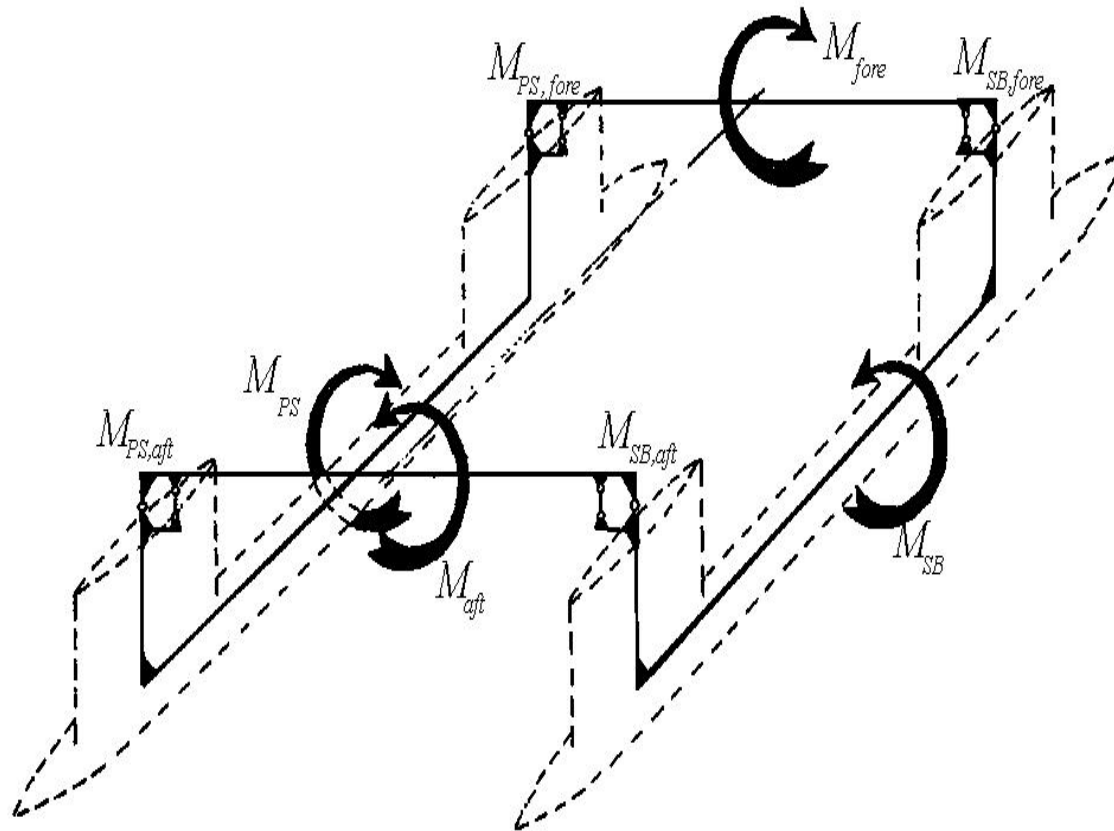


Today the relative vertical accelerations are recognized as the reason of the main part of transverse global loads of multi-hull ships with traditional hulls.

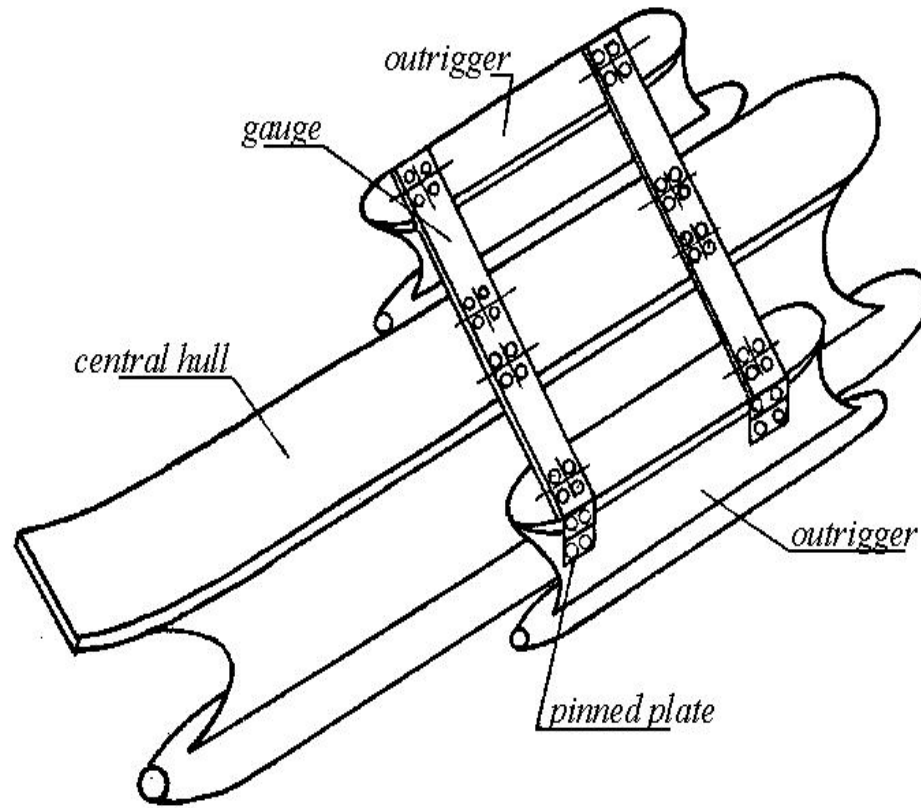
But the relative horizontal speeds are recognized as the reason of main part of transverse global loads of ships with small water-plane area.

For s semi-SWATH, two corresponded values of loads must be calculated and compared, and the bigger value can be used for estimation of such ships.

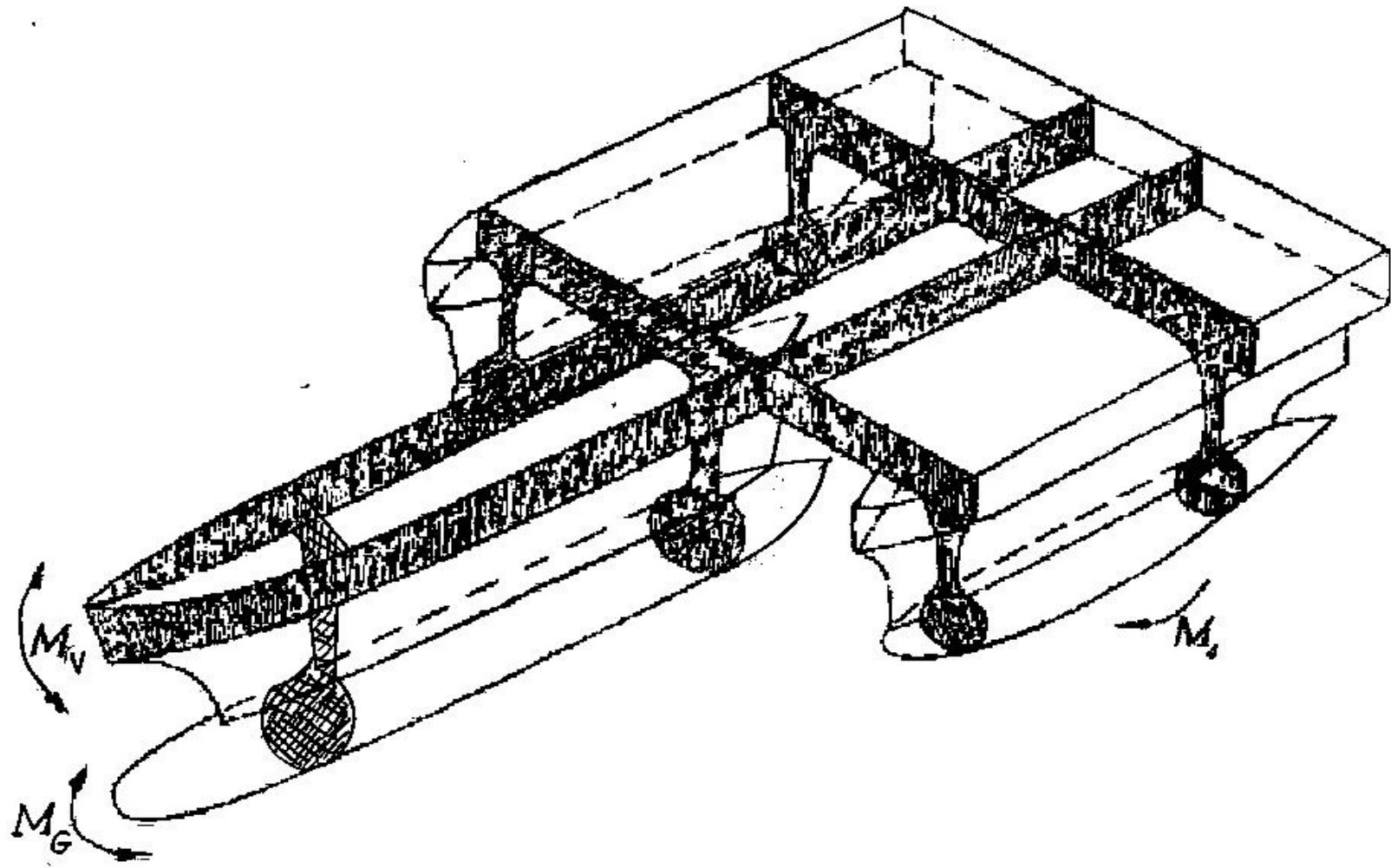
Measured loads on a SWATH model, [3].



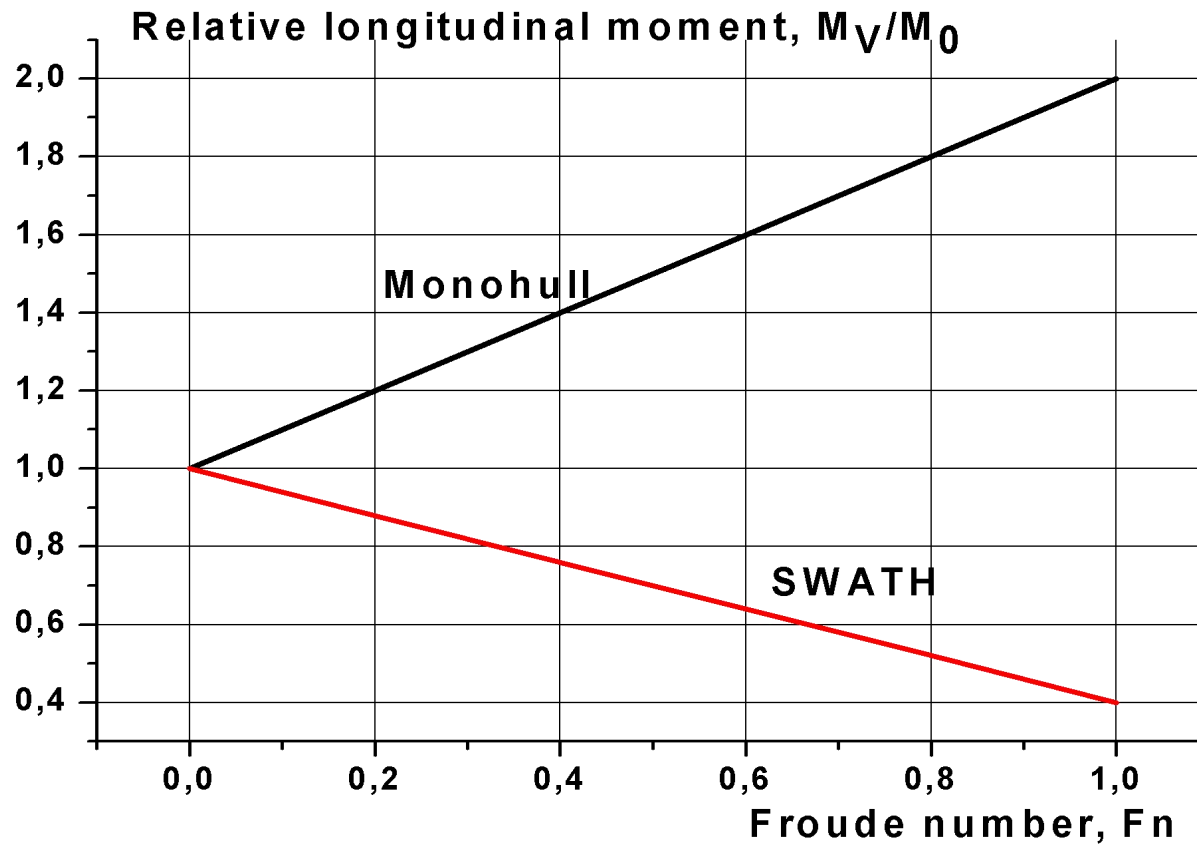
Tested outrigger SWA model, [3].



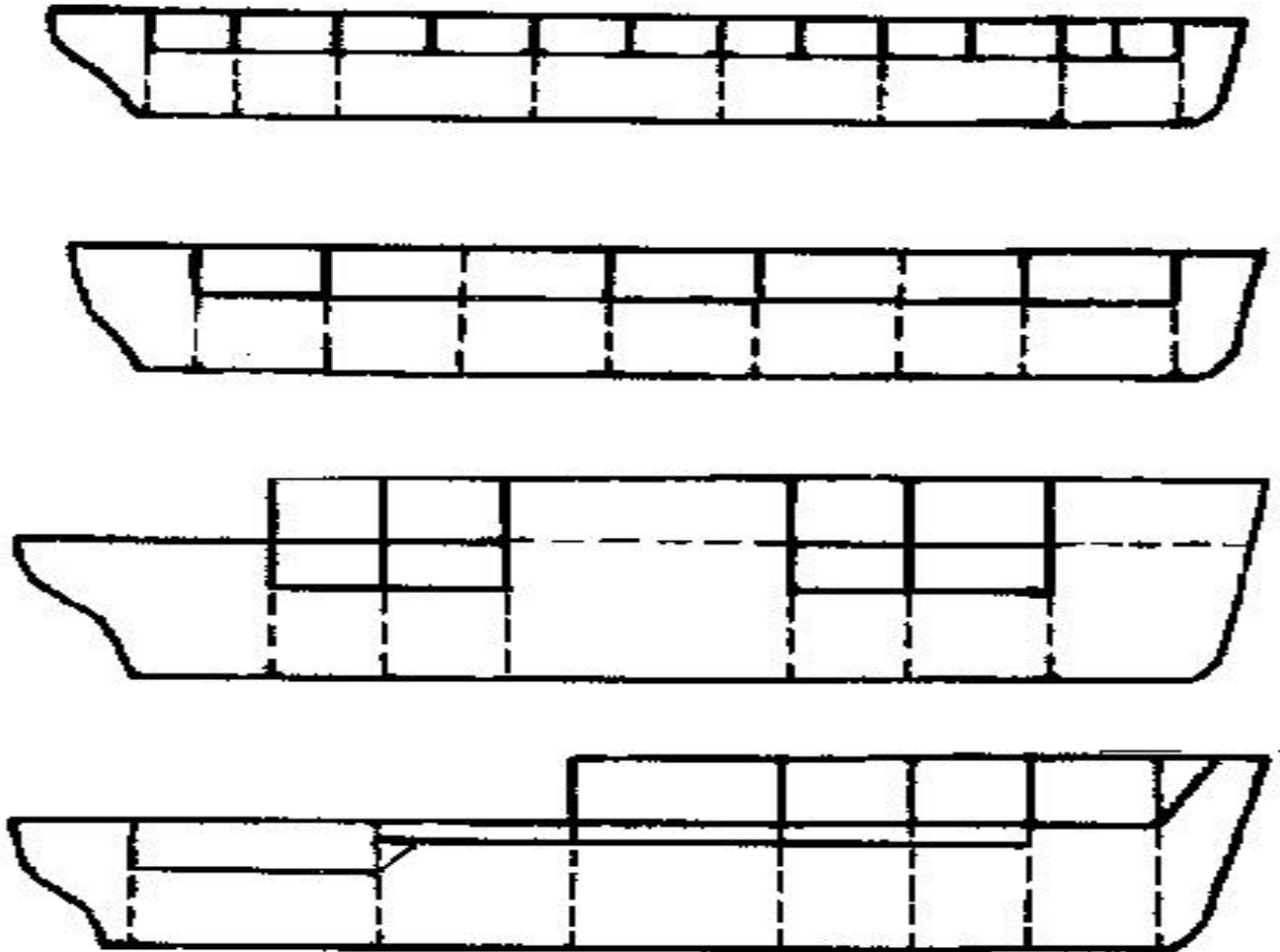
The main external loads and structure, a triple-hull SWA ship, [2].



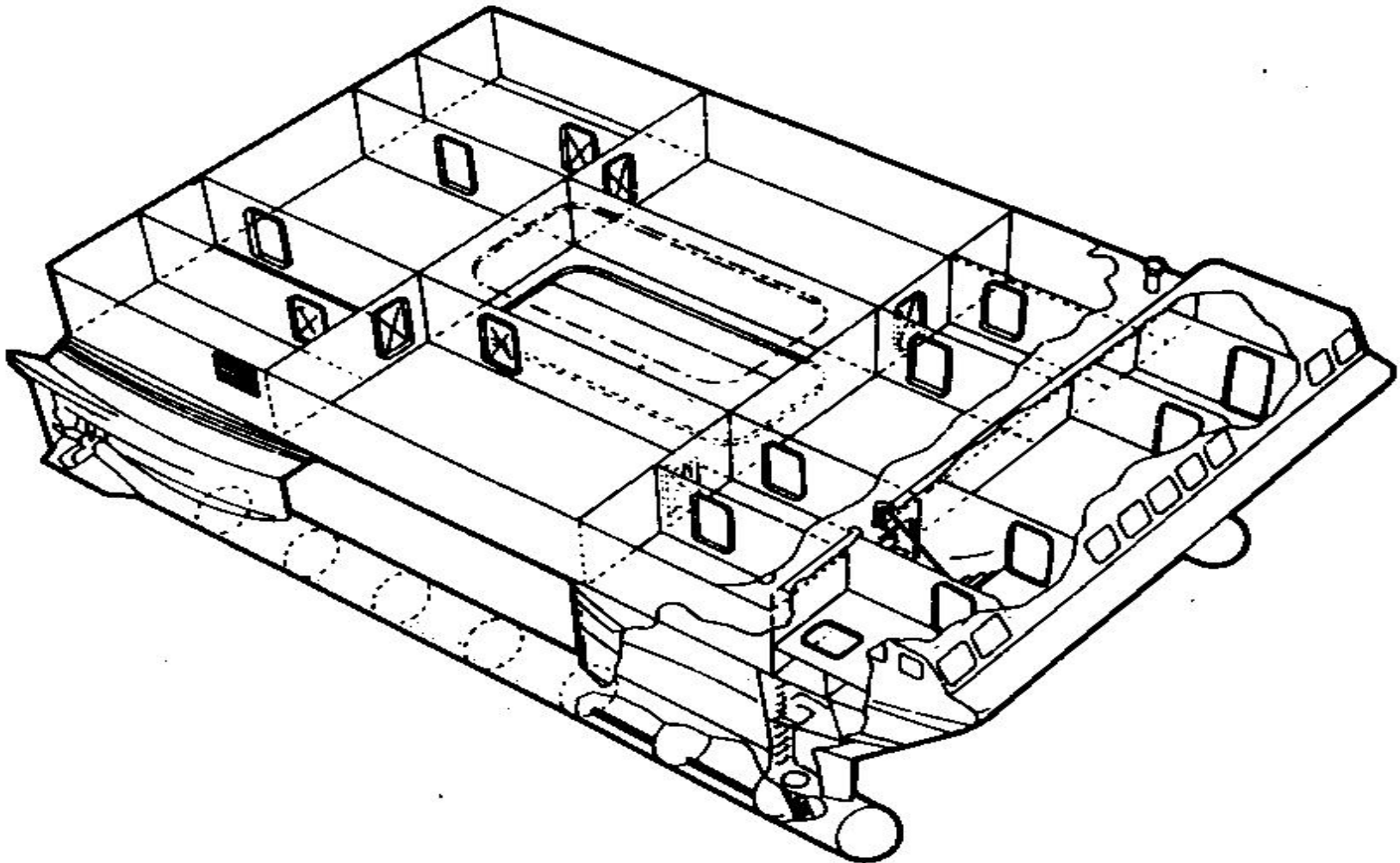
Longitudinal bending moment, [2].



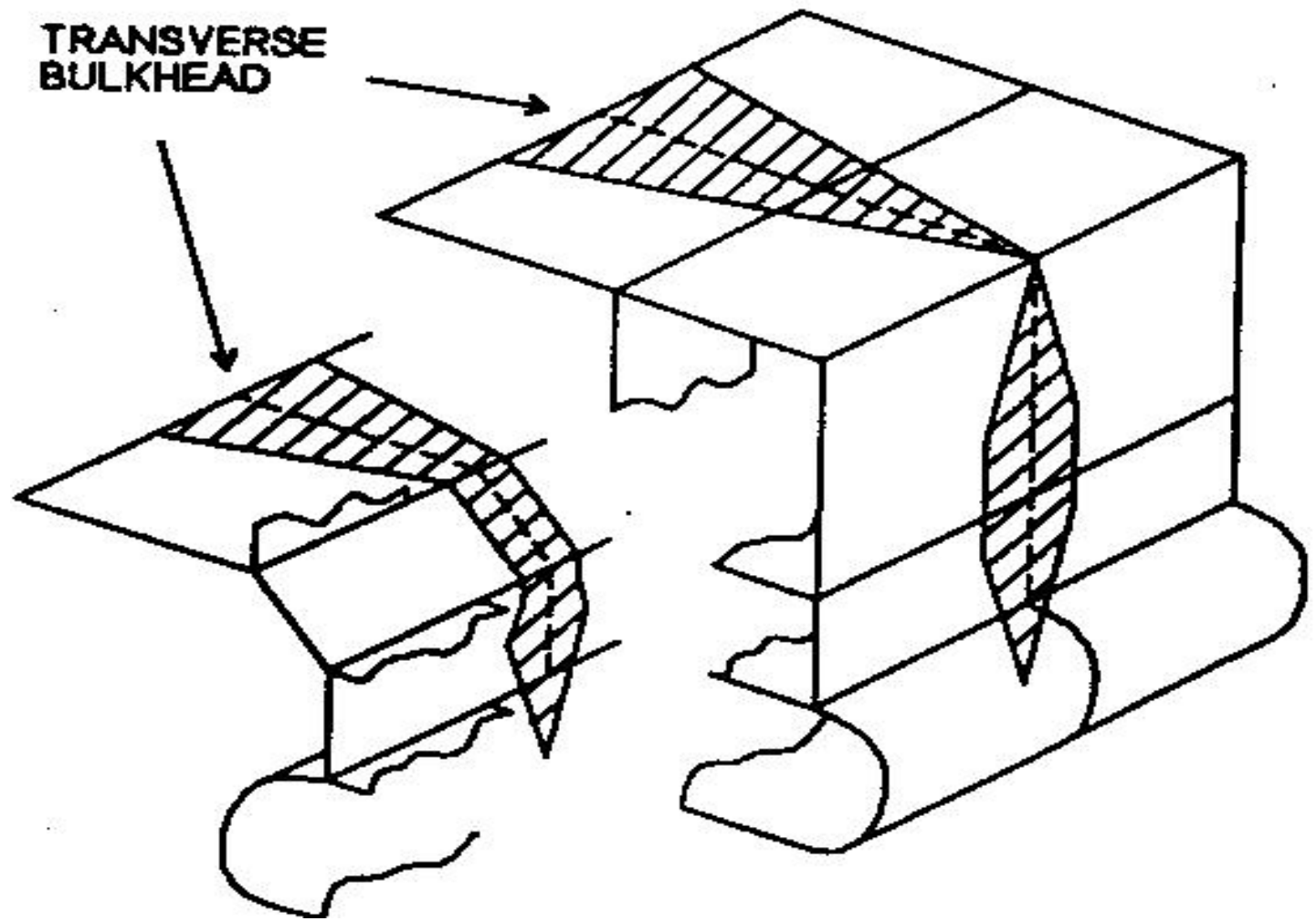
Options of platform structures: effective platform bulkheads must be supported by corresponded bulkheads in hulls, [3].



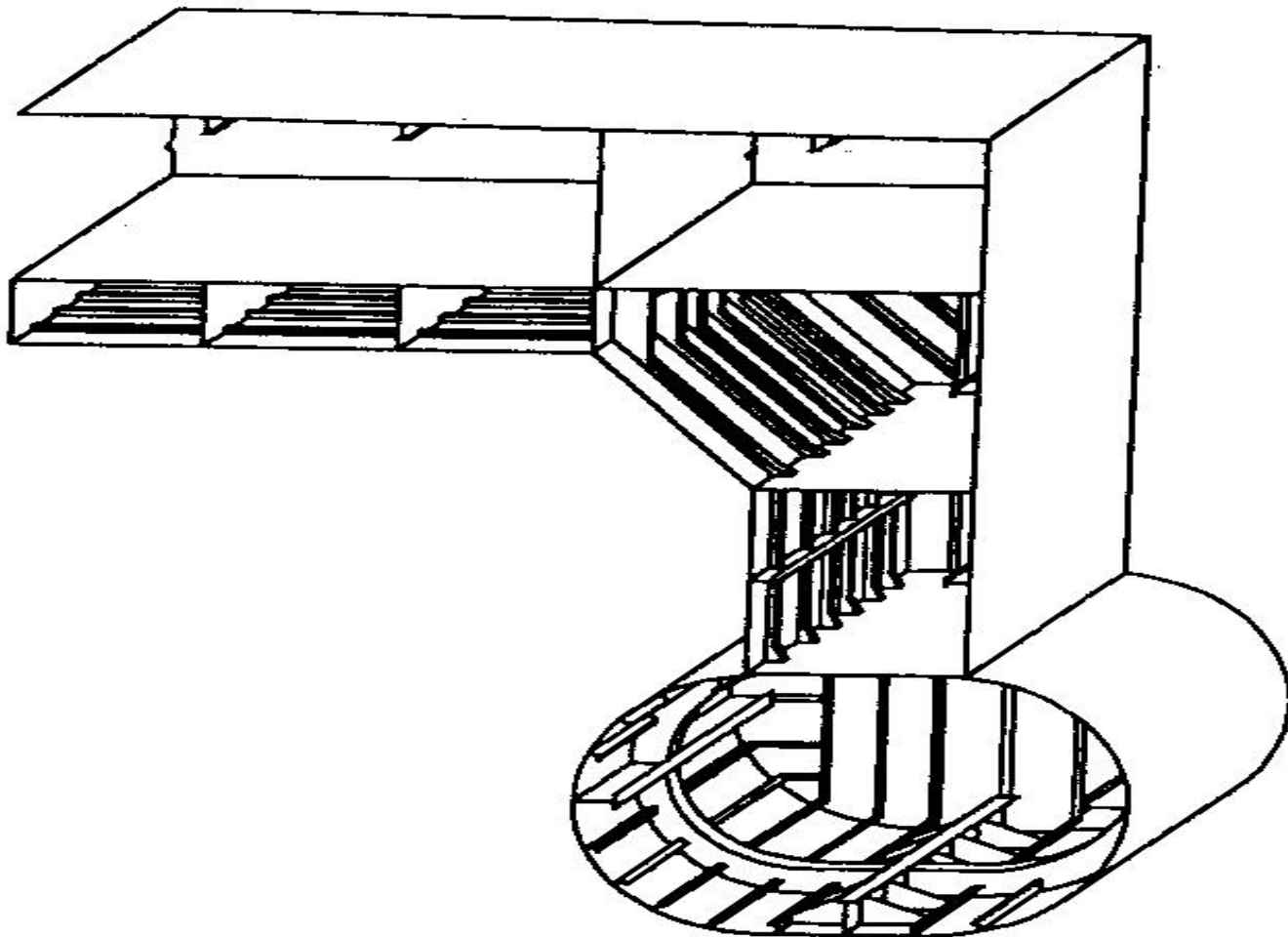
Structure of built trisecc “Kaimalino”, [3], (not supported bulkheads in the platform)



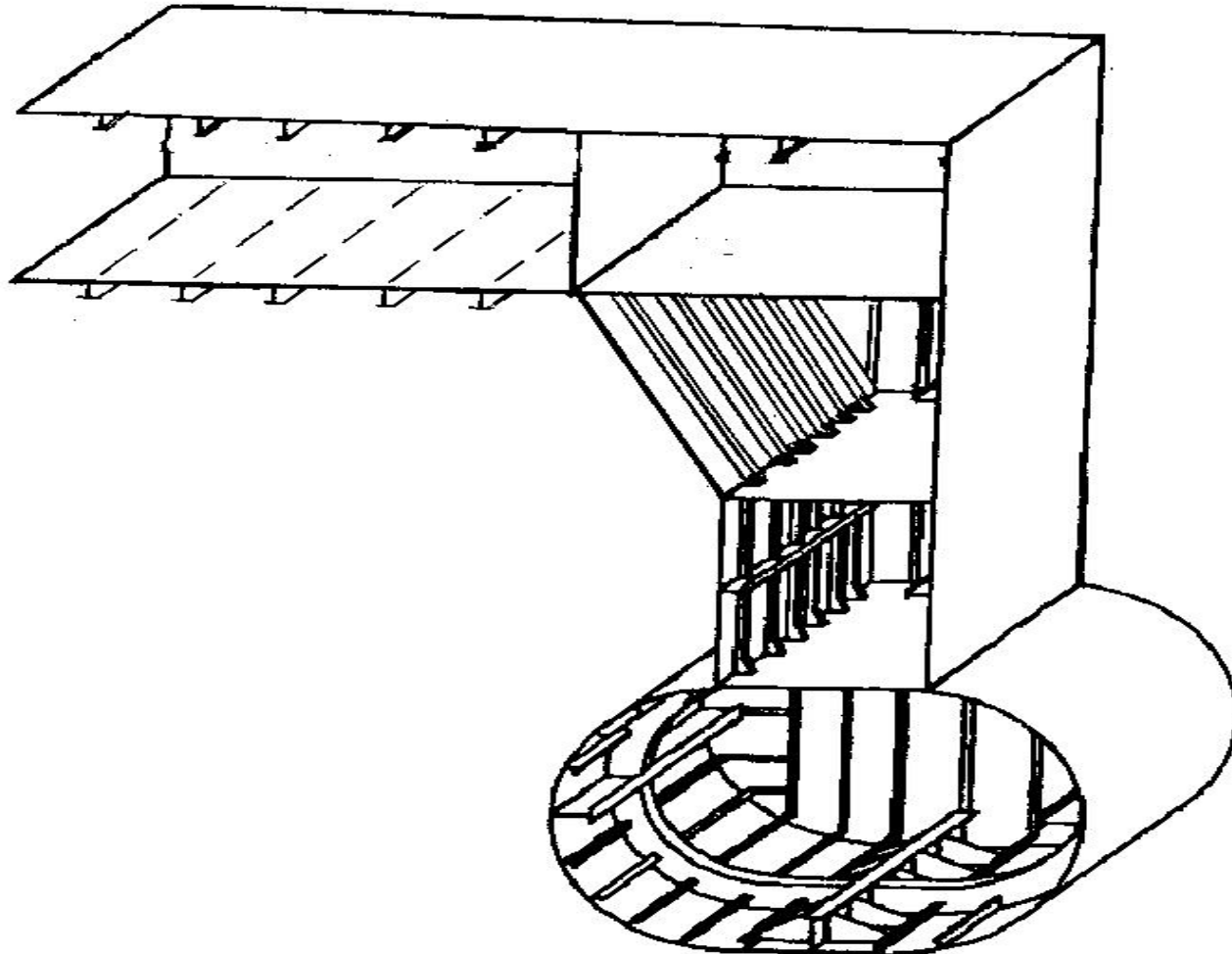
Effective band of transverse bulkheads of strut and platform, [3]



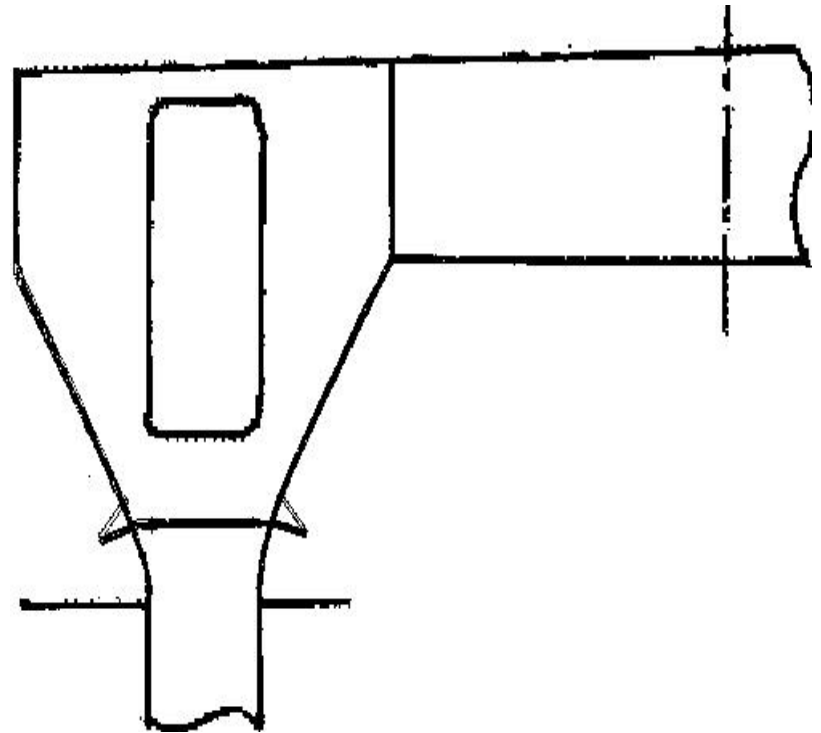
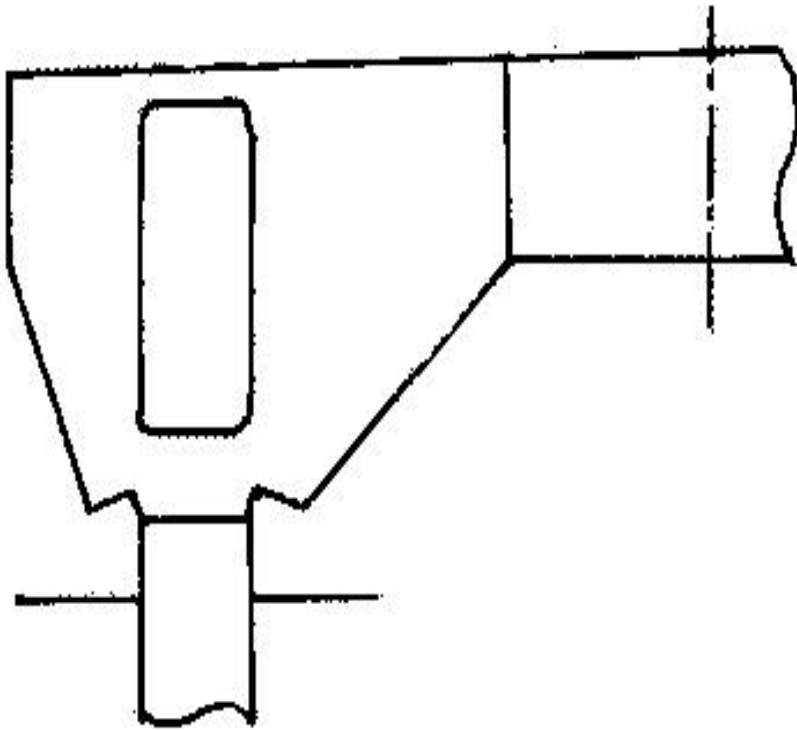
**Usual cross structure of platform, [3]
(with “second bottom” in the platform.)**



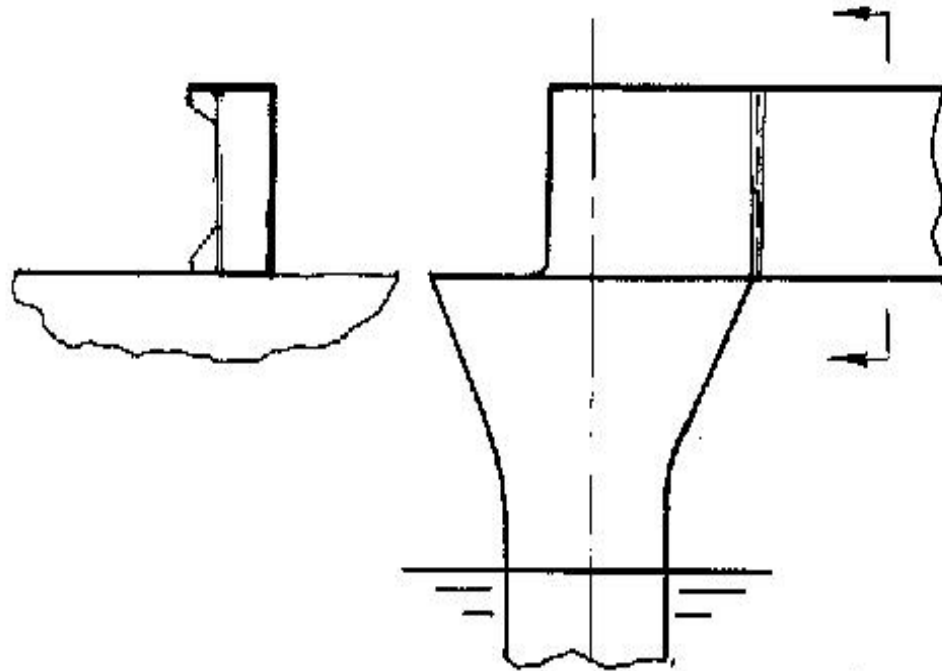
Developed structure of platform (without one plating), [3].



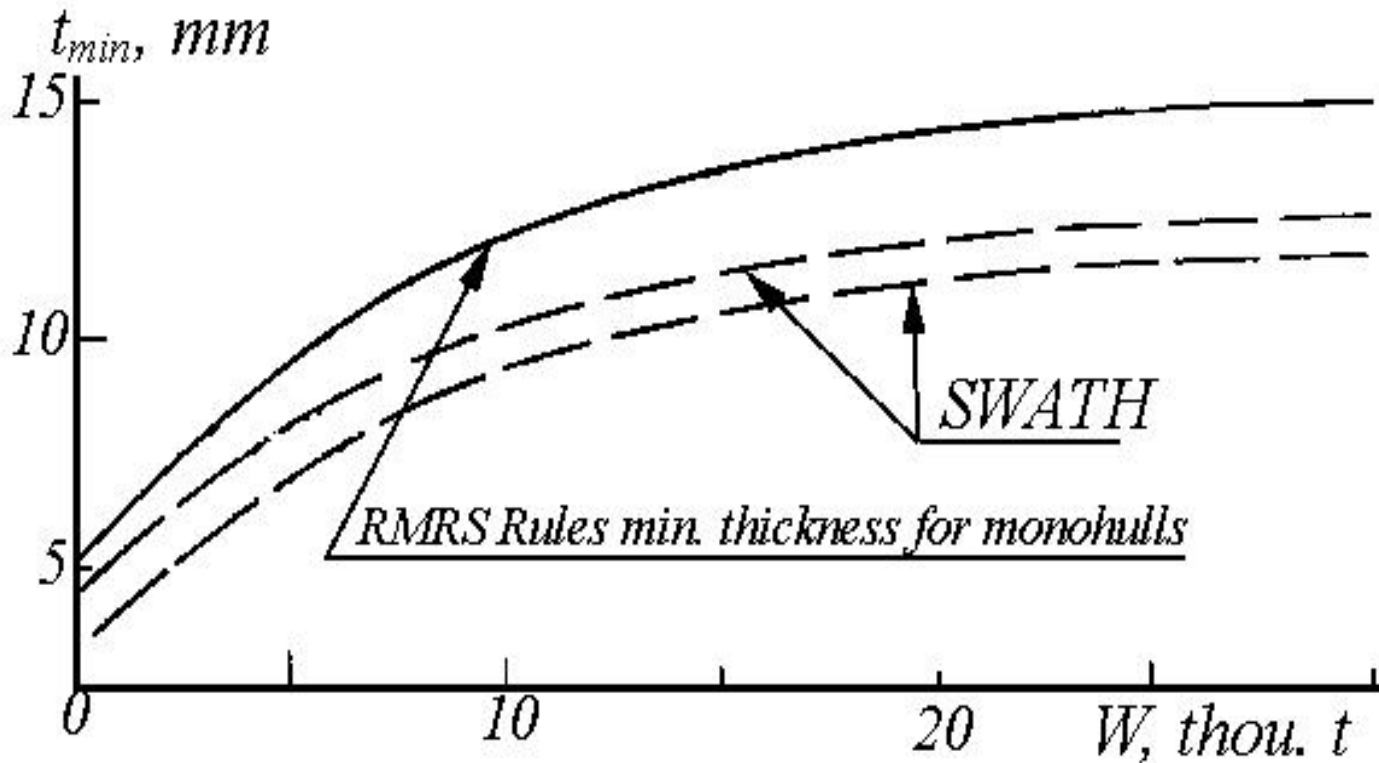
Bad (left) and better (right) bulkhead structure, [3].



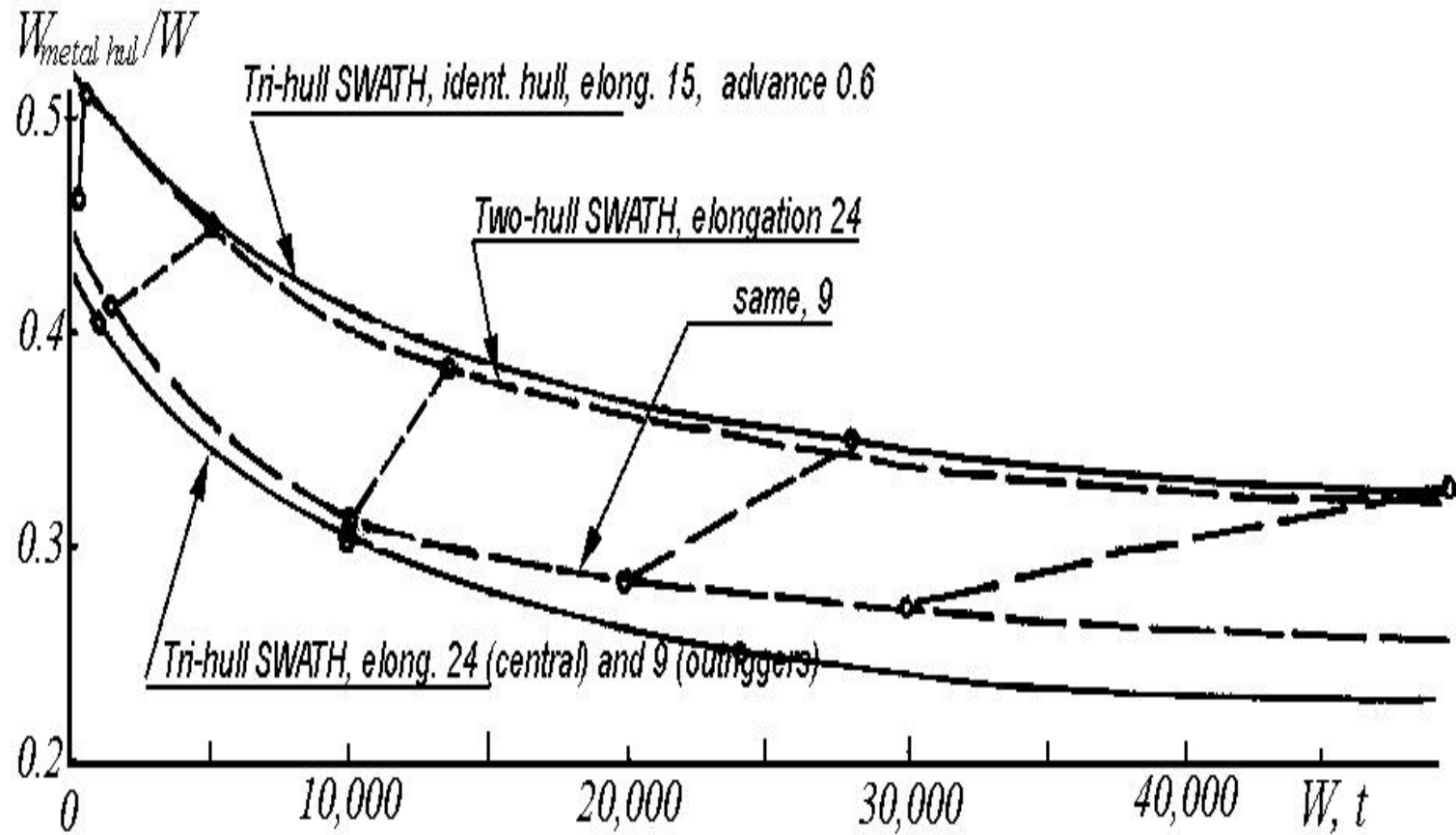
**Small-sized SWA hull connection
without “double-bottom” of platform: the transverse
strength is ensured by bulkheads only, [3].**



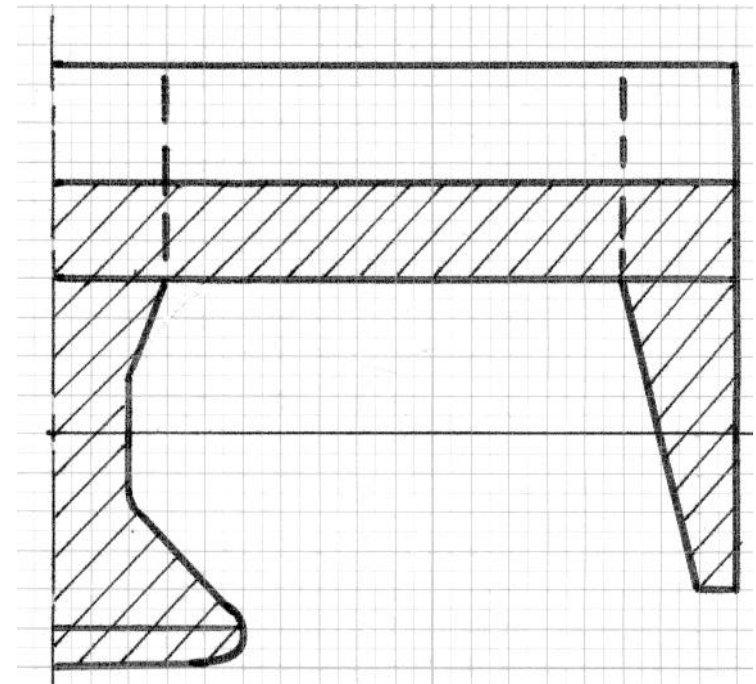
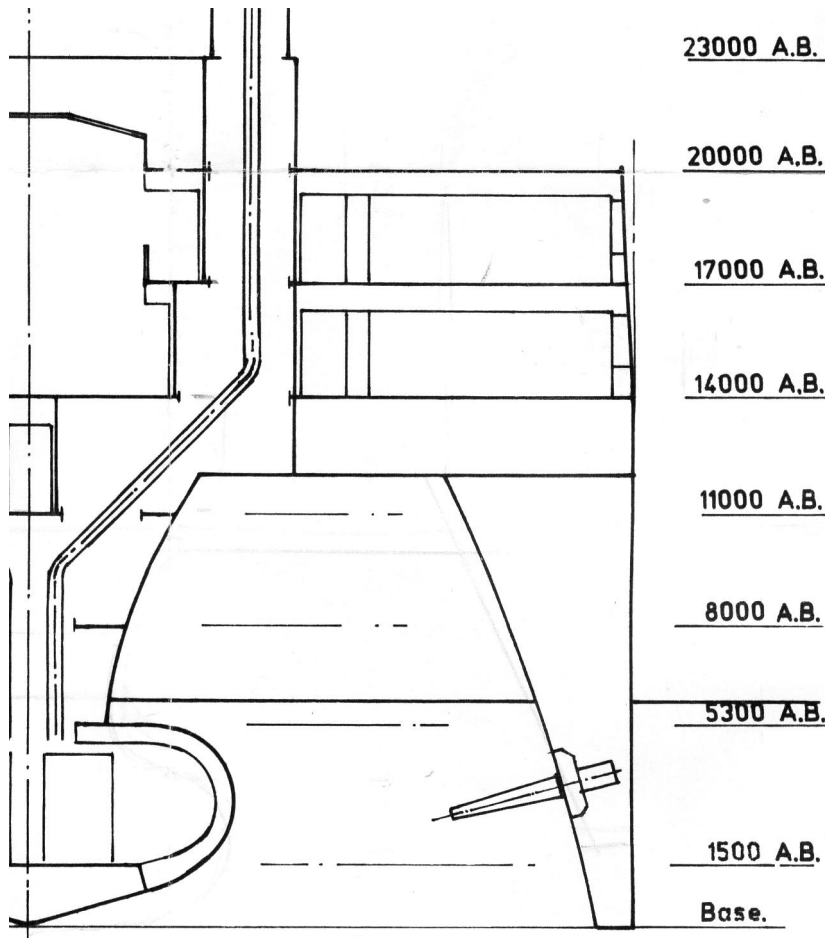
Minimal thickness of plating, [1].



Approximate estimation of hull relative mass, [1].



Cross section comparison: left – initial option, full displacement 6,000 t; right – alternative option, 4,500 t, [2].



REFERENCES.

1. Dubrovsky V., Lyakhovitsky A., “Multi Hull Ships”, 2001, *ISBN 0-9644311-2-2, Backbone Publishing Co., Fair Lawn, USA, 495 p.*
2. Dubrovsky V., “Ships With Outriggers”, 2004, *ISBN 0-9742019-0-1, Backbone Publishing Co., Fair Lawn, USA, 88 p*
3. Dubrovsky V., Matveev K., Sutulo S., “Small Water-plane Area Ships”, *Backbone Publishing Co., 2007, ISBN-13978-09742019-3-1, Hoboken, USA, 256 p.*