



TIDAL TURBINE FOUNDATION OPTIMISATION

RAMBOLL ENERGY
- RORY SINCLAIR

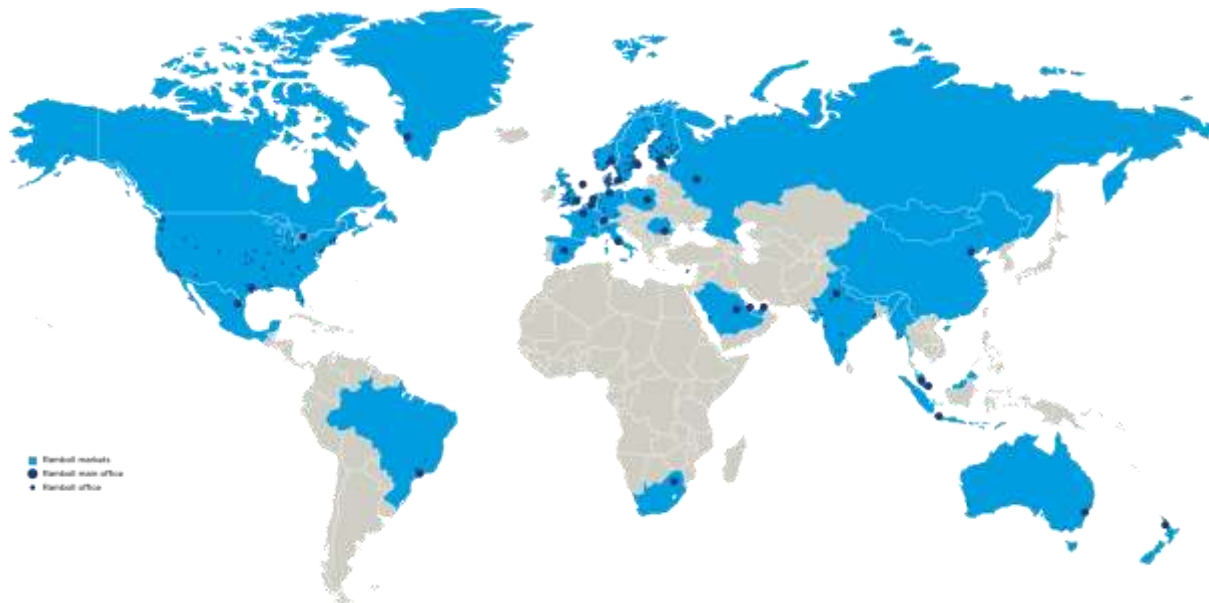
Presentation Contents

- Introducing Ramboll
- Tidal Turbine Foundations
- Our Experience with Fatigue in:
 - Gravity Bases
 - Floating
 - Bottom-Fixed (Jacket/Monopile/Duopod)
- Looking Ahead
- Summary

INTRODUCING RAMBOLL

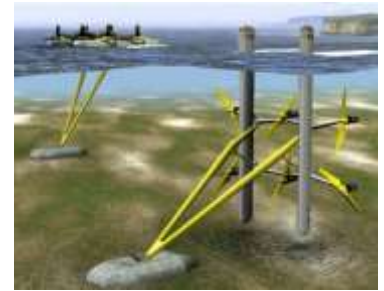
INTRODUCING RAMBOLL

- Ramboll: leading engineering consultancy company founded in Denmark in 1945
- Today, we employ more than 13,000 expert engineers and consultants
- 300 offices in 35 countries
- EUR 1.1 billion revenue
- Owned by Ramboll Foundation



INTRODUCING RAMBOLL

- O&G employees began first offshore wind project in 2001
- Since then...70% of all the world's offshore wind turbines now rise from foundations engineered by Ramboll
- Separate wind/tidal department set up 10 years ago
- 5 offshore offices: Denmark, Germany & UK
- London office next to Waterloo



TIDAL TURBINE FOUNDATIONS

TIDAL FOUNDATIONS

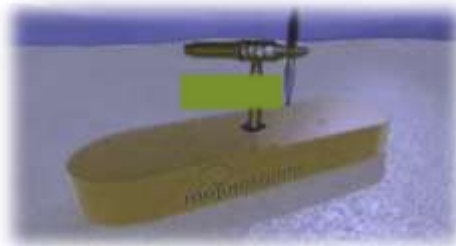
- Tidal energy faces huge challenges:
 - Installation costs
 - High current speeds
 - Rocky seabed
 - Uneven seabed
 - Limited access
- At present foundations are trials and so are not suitable for mass production
- The next stage is a repeatable structure



TIDAL FOUNDATIONS

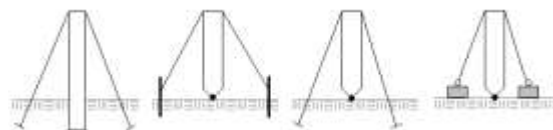
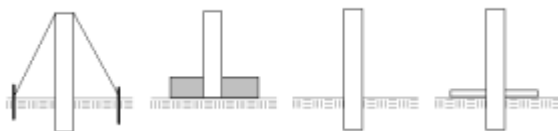
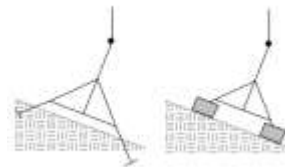
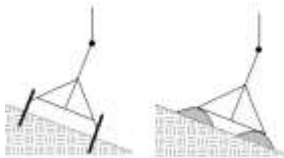
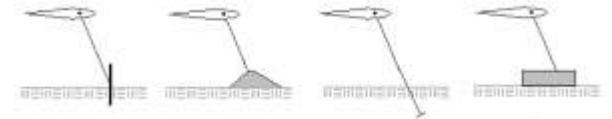
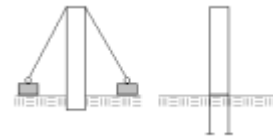
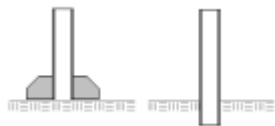
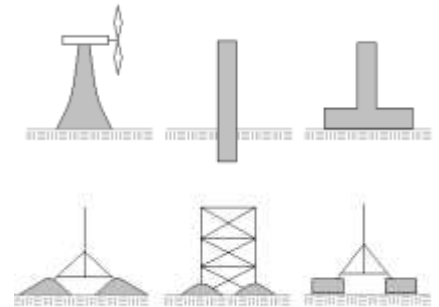
General Comments

- Progress your foundation design at earliest opportunity
- Design for fatigue, don't make it an afterthought
- Hire specialists if experience is not in-house
- Installation and foundation design are intertwined



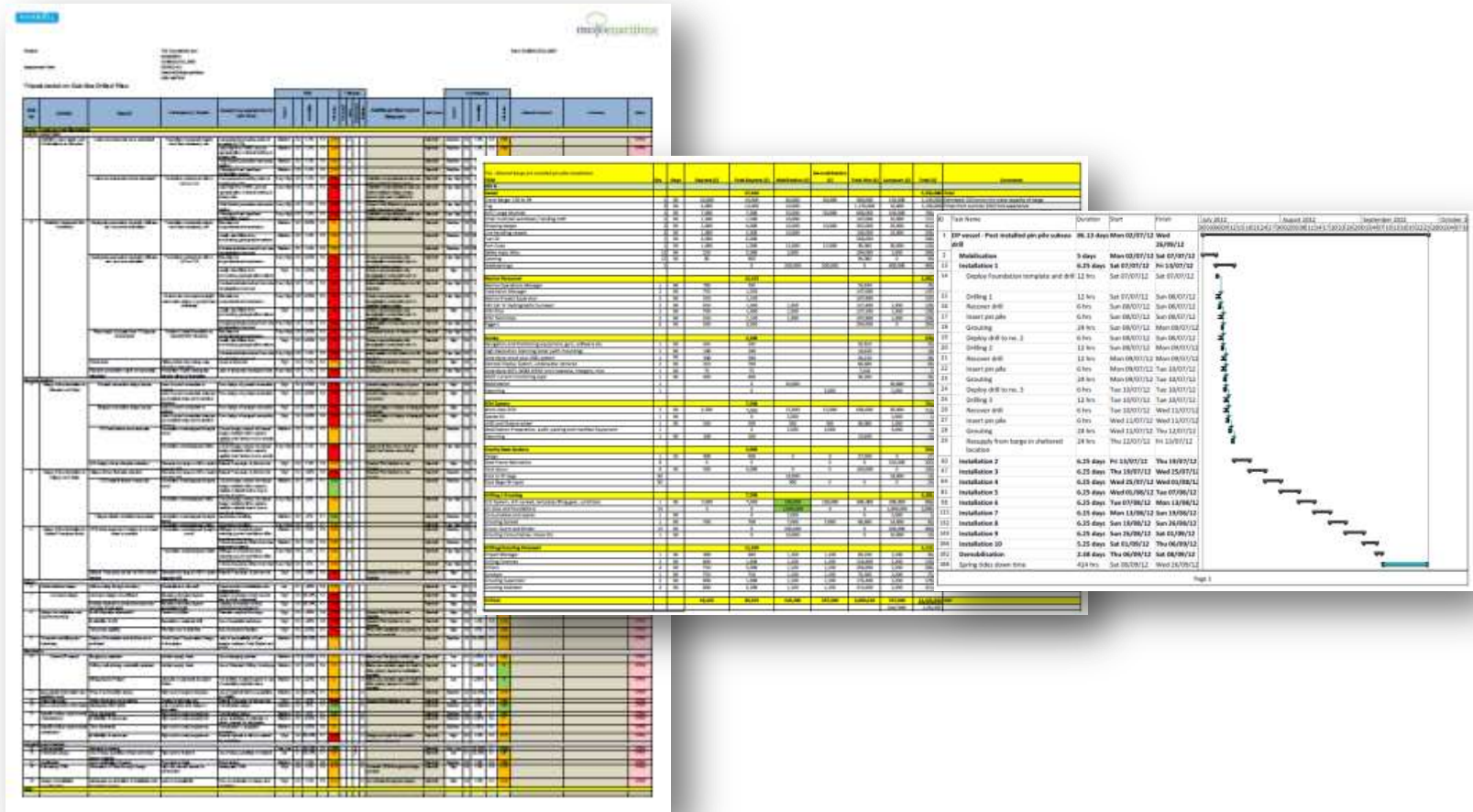
TIDAL FOUNDATION CONCEPTS

- Gravity Base
- Floating
- Bottom-Fixed



CONCEPT ELIMINATION PROCESS

Early-stage study of risk, cost and schedule

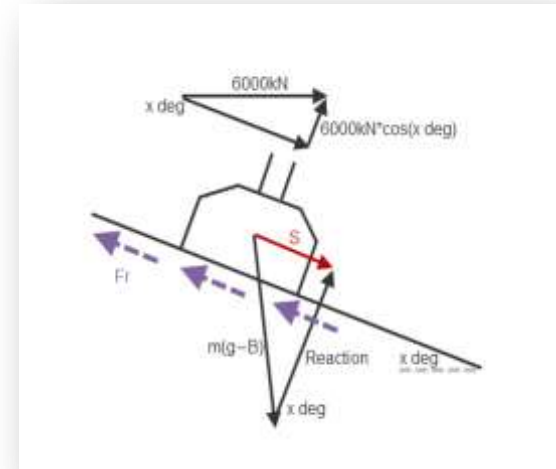
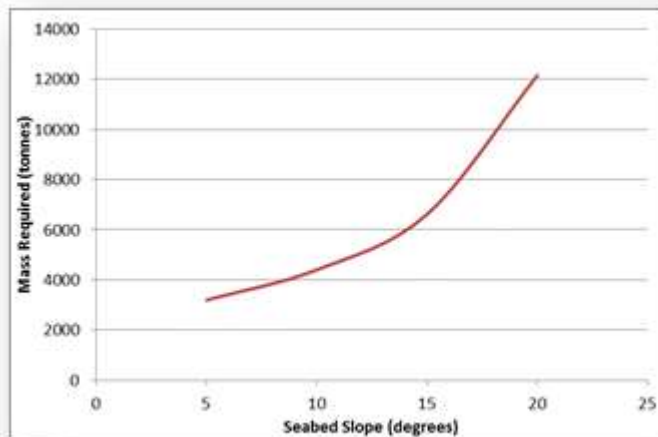
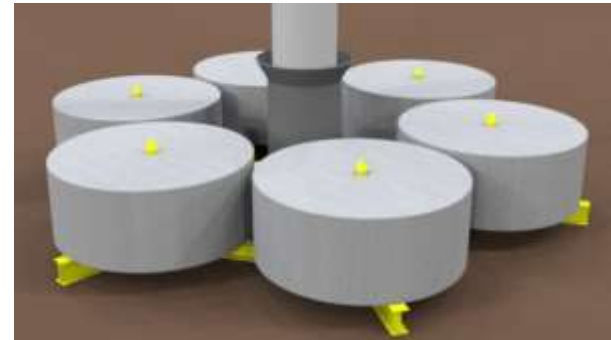


GRAVITY BASE

GRAVITY BASE

Problems:

- Substantial ballast mass required – v. expensive
- Carbon footprint large for ingots of steel/concrete
- Sensitive to seabed slope
- Bathymetry of tidal sites rarely flat



FLOATING

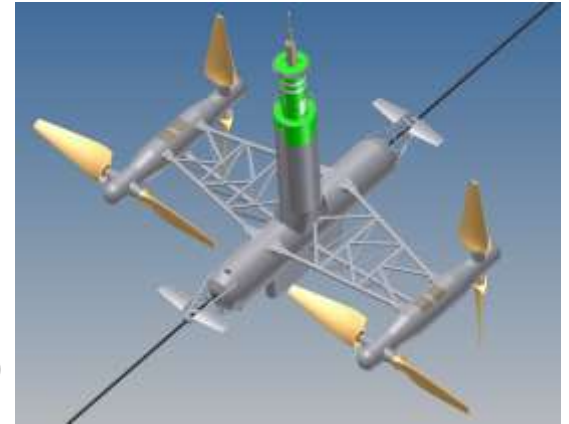
FLOATING

Pro's:

- Removes significant installation cost – hugely attractive solution economically
- Obvious O&M benefits

Other Thoughts:

- Still requires fixation by seabed anchor or rock socket (fixed)
- Introduces additional complexity:
 - Dynamic platform – impact on turbine efficiency
 - Dynamic export cable
 - Additional spacing requirements due to cables



MONOPILE

MONOPILE – DESIGN

General

- Simple design, proven concept
- Simple fabrication, weld automation

Fatigue Considerations

- Material thickness/diameters governed by fatigue
- ULS utilisation ratios are low
- No fatigue sensitive joints
- Pile diameter at upper limit of drilling capability...



MONOPILE - INSTALLATION

Subsea Drilling

- Most tidal sites have rock ground conditions – this requires drilling
- Current drilling diameter limit of $\sim >2.8\text{m}$ (installed pile less than that)
- For 1MW+ device, MP's may struggle to work in fatigue at this diameter



MONOPILE - INSTALLATION

Topside Drilling

- No such diameter limits BUT requires a stable platform e.g. a jack up barge:
 - Successful application of jack ups in tidal races is limited (stability & VIV issues)
 - Jack up owners reluctant to deploy in tidal races
 - Susceptible to weather downtime
 - Expensive day rates
- Bottom line:
 - If “no” to jackups → it’s a “no” to topside drilling
 - For 1MW+ → very possibly a no to MP’s

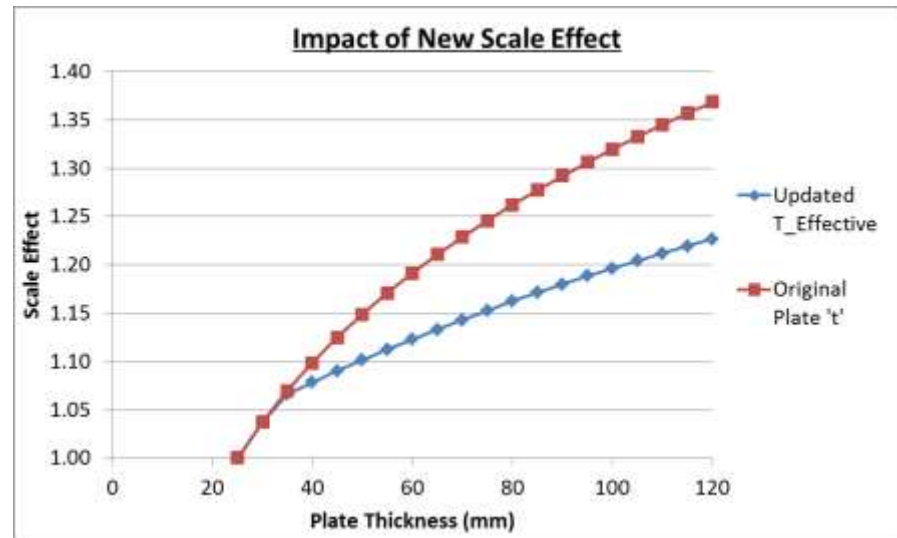
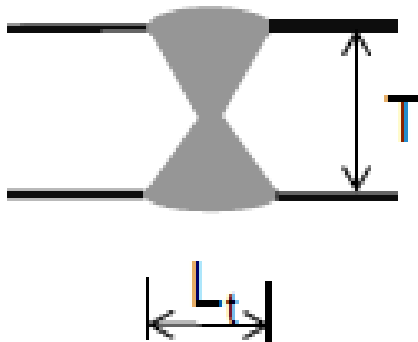


MONOPILE – A REVIVAL?

Updated Scale Effect

- SN curves derived using test plate thickness 25mm
- Scale effect used to account for actual plate thickness (basically a factor applied to the stress term)
- Formulae changed to depend upon weld width

$$\log N = \log \bar{a} - m \log \left(\Delta \sigma \left(\frac{t}{t_{\text{ref}}} \right)^k \right)$$



MONOPILE – A REVIVAL?

Updated SN Curves

- Current SN Curves:
 - Based on decades old research
 - Questionable representation of modern materials
 - Questionable representation of advances in modern fabrication techniques
 - Questionable representation of current member geometries (7m + diameter!)
- Structural Lifetime Industry Collaboration (SLIC):
 - Joint-industry project
 - Develop the existing SN curves
 - New testing being carried out using modern materials/practices/geometries
- Potential for improvement in fatigue performance of MP (or otherwise...)

MONOPILE – VIABLE?

Summary:

- Current diameter restrictions severely limits application of the MP
- < 1MW devices (prototype?) – likely to be viable
- > 1MW devices - potentially going to have fatigue issues
- Codes are changing as we speak, FLS failure not necessarily the case in the future...
- If MP's can be made to work in fatigue with OD limits they may be 'the solution'

DUPOD

DUOPOD

- Significant reduction in pile diameter due to:
 - X2 load paths to support (soil)
 - Forces are more 'axial'
 - Capacity of soil to 'take' axial load greater than lateral load
- Problems:
 - Joints introduced – suddenly much more complicated for fatigue
 - If significant out-of-plane bending loads at joints - fatigue issues
 - More expensive to fabricate than MP
- Are there better solutions?

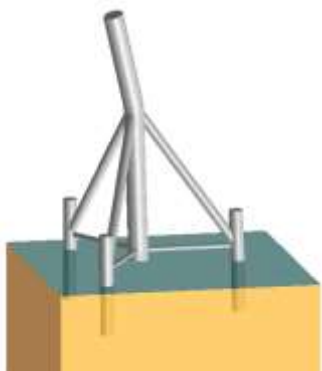


TRIPOD

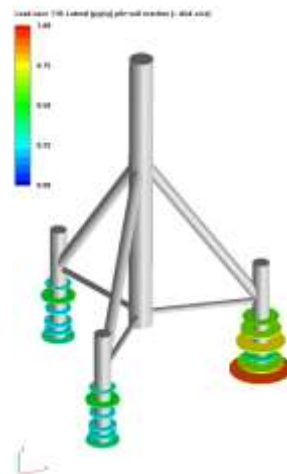
TRIPOD



- Main advantage of duopod without going all the way to a jacket
- 3rd leg reduces out-of-plane bending forces in joints
- Potentially thinner sections than with duopod
- Advantage of on-bottom stability
- More expensive to fabricate than MP
- The solution we often settle upon



RAMBOLL



JACKET

JACKETS

Key Points

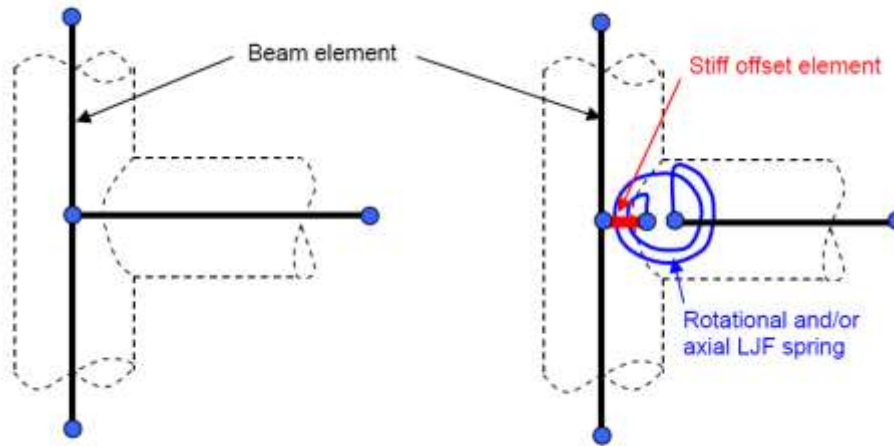
- Lever arm to load not sufficient to 'require' a jacket
- Multiple piles -> increased installation complexity
- Lots of members -> fabrication complexity & cost (very much)
- Probably not the economic answer
- May be deployed at deeper water sites in future



LOOKING AHEAD

Super-Elements & Influence Matrices

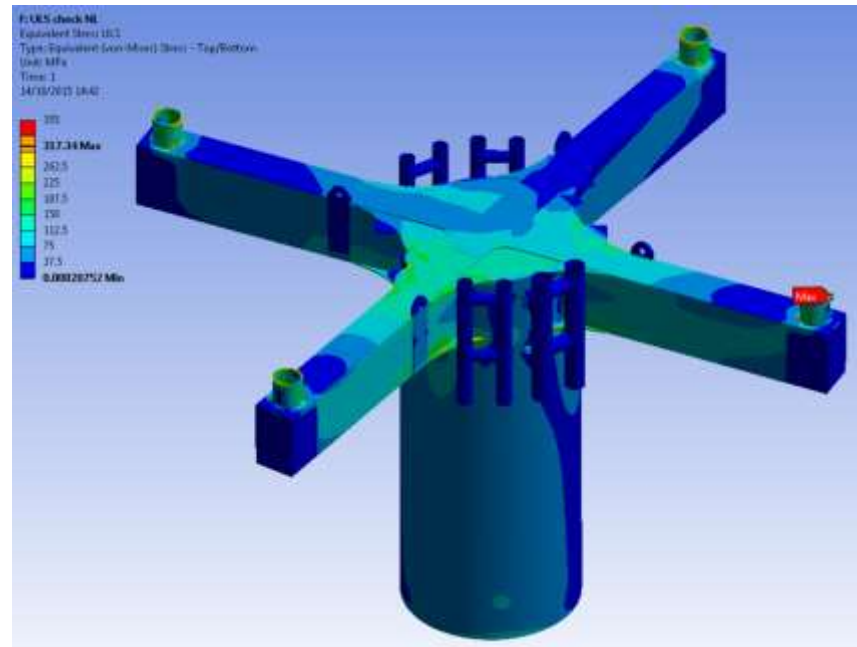
- Simple Beam Element Model (BEM) simplifies stiffness @ joints (below left)



- Local Joint Flexibility (LJF) introduced at simple joints as more accurate representation of joint stiffness
- Involves insertion of offset (very stiff element) and a spring to model joint stiffness
- EFTYMOI parametric equations empirically derived to determine LJF
- Generally (though not always!) results in improvement in fatigue performance

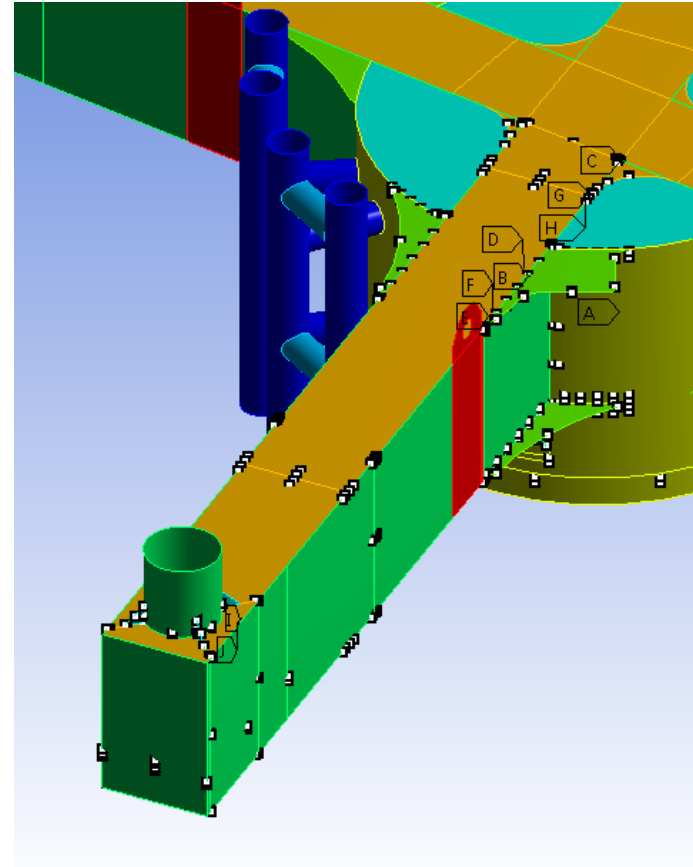
Super-Elements & Influence Matrices

- Equations are not suitable/reliable for complex joints e.g. offshore substation girder joint
- We use super-elements instead!
- What is a super-element:
 - We create accurate model of our complex geometry in FE software
 - Extract stiffness & mass matrix and insert into same old (simple) beam element model
 - Seamless integration with BEM software



Super-Elements & Influence Matrices

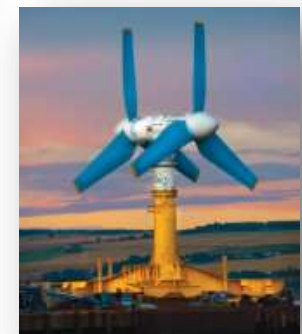
- Influence Matrices:
 - Relates forces in simple BEM with forces inside the super-element 'black box'
 - Basically a large matrix of numbers
- A few years ago influence matrices mainly used in very complex joints
- Their use is no-longer exceptional:
 - We're now inserting influence matrices wherever we see a benefit
 - Even within applicability limits of EFTYMOI equations
 - Getting joints to 'work' that we just couldn't get working



SUMMARY

Summary

- Foundation design and installation intertwined, foundation design impacts installation – a major project cost driver
- Tidal foundations are almost always governed by fatigue
- There is no one foundation solution, we don't subscribe to the 'universal foundation' concept:
 - When you progress a detailed design at array scale, one size fits all isn't economic
 - Turbine & site-specific variables easily justify expense of optimised foundation
 - Cluster foundations at array scale
 - Our fee is negligible 😊



THANK YOU